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PRECISE POINT POSITIONING

PART 2: A DEEPER DIVE



Tuesday, April 14, 2015

1 pm–2:30 pm PDT

2 pm–3:30 pm Mount

3 pm–3:30 pm Central

4pm–5:30 pm Eastern

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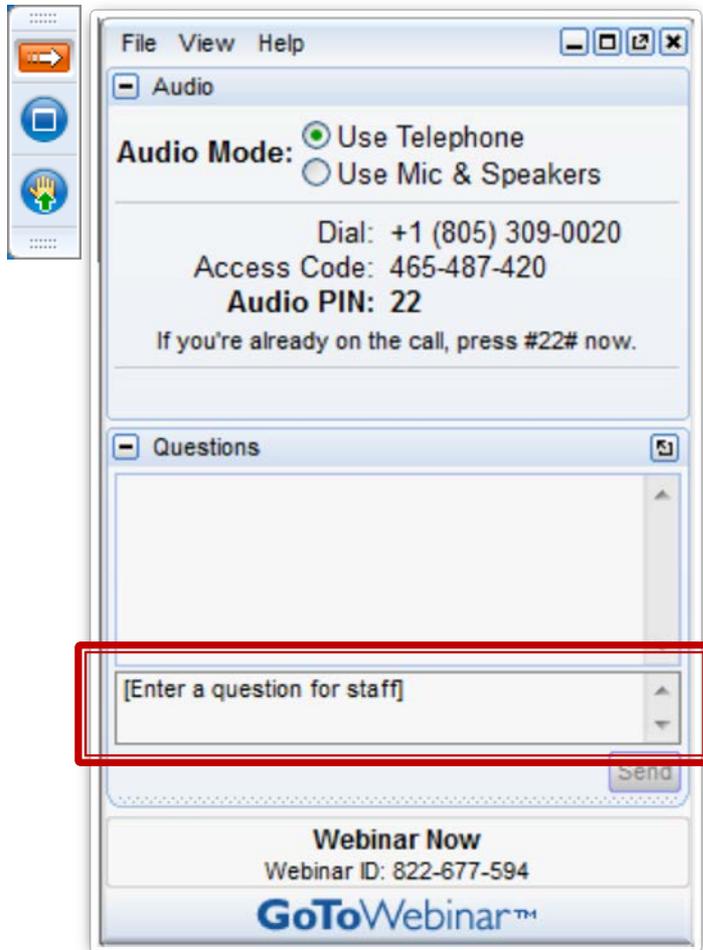
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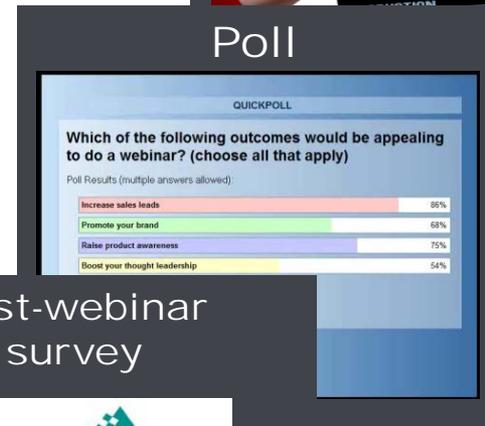
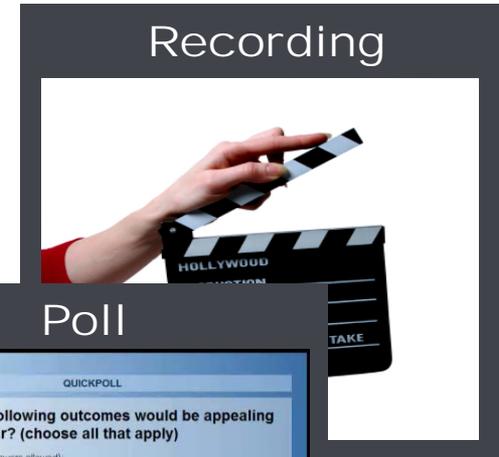
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A diverse audience of over 600 professionals registered from 50 countries, 29 states and provinces representing the following industries:

23% GNSS Equipment Manufacturer

23% Professional User

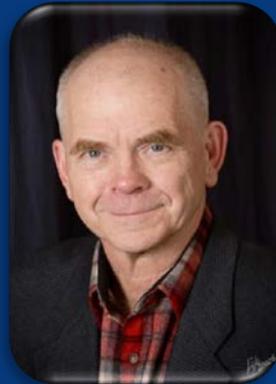
12% System Integrator

15% Product/Application Designer

27% Other



Welcome from *Inside GNSS*



Glen Gibbons

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A word from the sponsor



Thomas Morley
M.Sc, M.E., P.Eng.
Manager
Applied Technology
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NovAtel, Inc

Precise Point Positioning - Part 2: A Deeper Dive



Demoz Gebre-Egziabher
Aerospace Engineer and
Mechanics Faculty,
University of Minnesota

Poll #1

In next year or two PPP services will be available to all(choose one)

- On all GPS/GNSS receivers (e.g mobile, surveying, etc)
- Retrofitted to all receivers
- On newer high-end receivers only
- What is PPP?



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Receiver Considerations for High-Accuracy Applications

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Sanjeev Gunawardena
Research Assistant Professor
Air Force Institute of Technology

Receiver Type → Design Parameters ↓	Mass Market / Consumer	Aviation Grade / Machine Control	Geodetic / Reference Station
Antenna Type Coverage Bands Approximate Size	Passive chip or helical element Covers L1 bands (GPS, GLONASS) Surface Mount Package <2cm 	Patch on controlled dielectric single element (L1 band) or Stacked (L1 and L1/L5 bands) Integrated diplexer and LNA 10 cm 	Multipath Limiting Elements Stable Phase Center External Choke Ring Design In-system calibration of inter-channel biases 30 cm 
GNSS Bands	GPS L1 C/A, and GLONASS L1 and/or BeiDou B1 SBAS on L1	GPS L1 C/A GPS L5 SBAS on L1 and L5	GPS L1 C/A, P(Y)* GPS L2 C, P(Y)* GPS L5
Pre-correlation Bandwidths	<2MHz (GPS C/A) <2 MHz (GLONASS)	4-16 MHz (L1) 16 MHz (L5)	16-24 MHz (L1, L2, L5)
Sample quantization and effective sample data rate (Mbytes/sec)	1 or 2 bits/sample 0.5-1.0	2-4 bits/sample 8-32	2-8 bits/sample 24-150
Pre-Correlation Interference Detection/Suppression	none	CW, Swept CW, FM Non-uniform quantization J/N meter	Pulse-suppression, notch filter, frequency-domain excision
Reference Oscillator Type and stability	TCXO ($\leq 10^{-6}$)	High-performance TCXO or OCXO ($10^{-6} - 10^{-7}$)	OCXO or atomic standard (10^{-9})

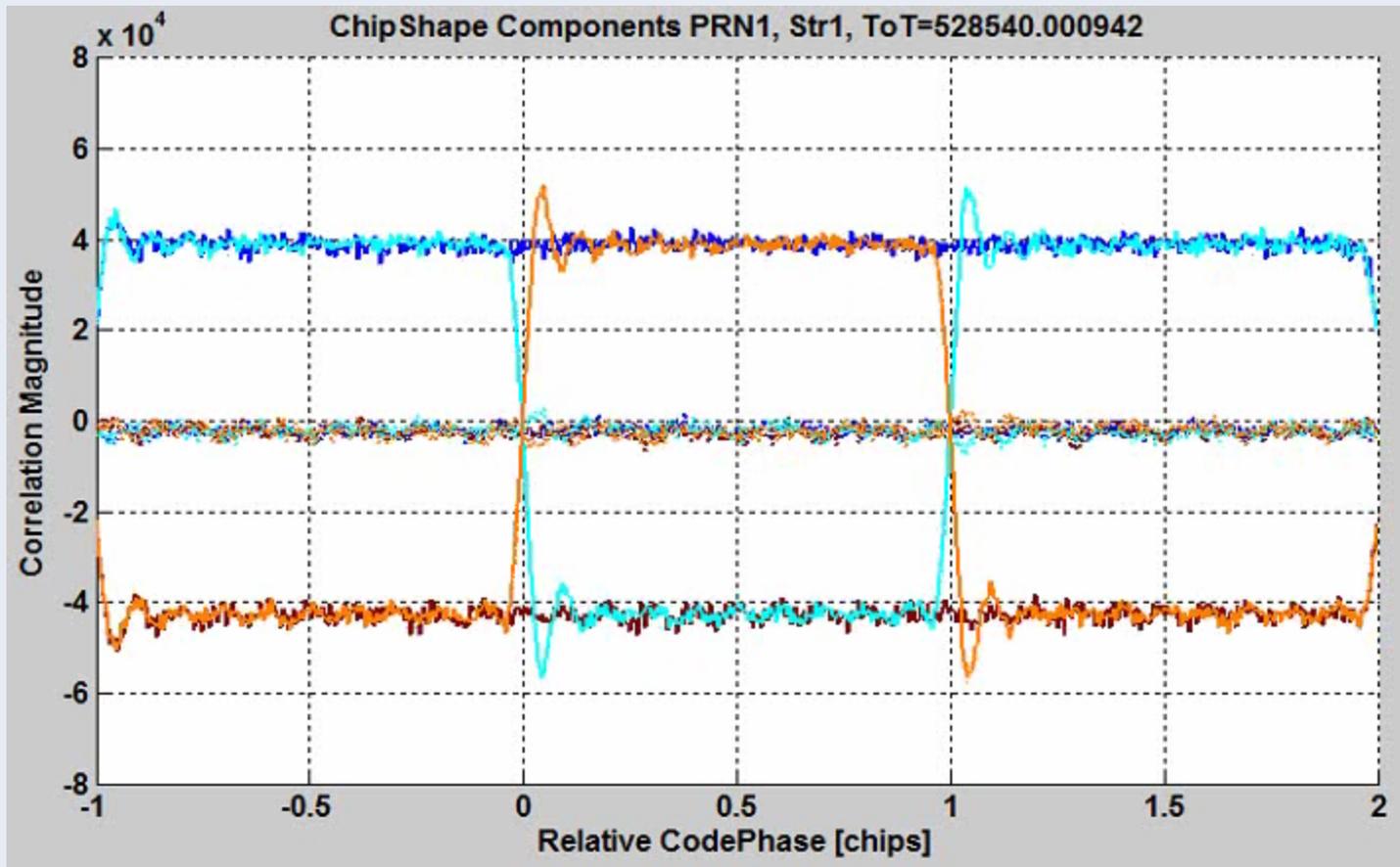
* Using codeless or semi-codeless tracking techniques

Review: Baseband Processing Comparisons

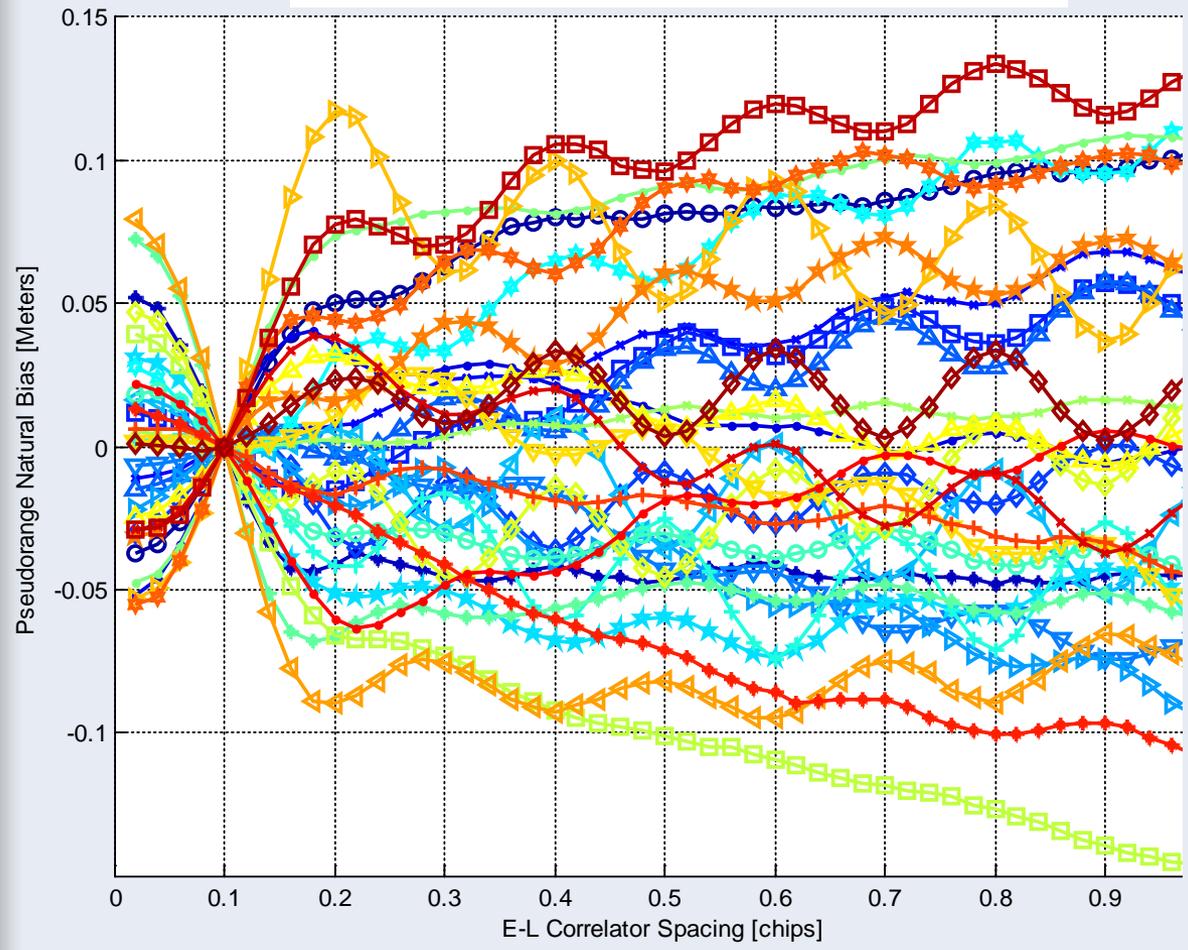
Receiver Type → Design Parameters ↓	Mass Market / Consumer	Aviation Grade / Machine Control	Geodetic / Reference Station
Carrier Tracking Architecture	None (A-GNSS) FLL (standalone GNSS)	FLL-assisted PLL or PLL (inertial aiding)	PLL (ephemeris aiding)
Code Tracking Architecture	None (A-GNSS) carrier-aided DLL (standalone)	carrier-aided DLL	carrier-aided DLL
Multipath Mitigating Technology	none	Narrow-correlator Double-delta correlator	Narrow-correlator Double-delta correlator Multi-correlator estimation
Typical Early-Late Correlator Spacing (GPS L1 C/A Chips)	1.0	0.3-0.1	0.1-0.01
Inter-Channel Pseudorange Bias Correction (Primarily for GLONASS)	None OR Model-wide calibration table	Device-specific calibration table (part of device testing and qualification process)	Dynamic calibration
Other features	Massive banks of parallel correlators for 'flash acquisition and long coherent integration	Dynamic multipath estimation and mitigation	Interference and signal deformation monitoring
Typical Implementation (2015)	System on chip (SOC) ASIC with integrated RF and baseband (standalone)	2-ASICs (RF + Baseband) Single SMD module or card	Front-end: RFIC-based Baseband: ASIC or FPGA + embedded processor
Power consumption and Cost	<2 W < \$3	<20W \$300-\$3,000	>30W \$6000-30,000

- Receiver Considerations for High-Accuracy Applications
 - Nominal Signal Deformation
 - Front-End Component Effects
 - Multipath
 - In-Band Interference: detection and mitigation

- Extension to GNSS
 - GLONASS inter-channel biases
 - High-Accuracy GNSS Receivers: what to expect in coming years



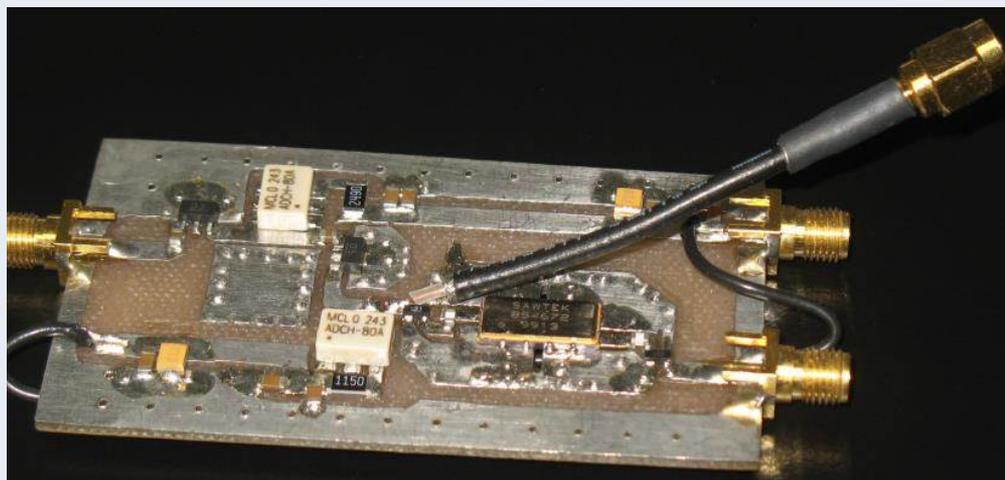
GPS-SPS Pseudorange Natural Biases



- PRN01, SV63, Block IIF, EI:57, Pdi:400s
- ◆ PRN02, SV61, Block IIR, EI:69, Pdi:210s
- PRN03, SV33, Block IIA, EI:69, Pdi:400s
- ◆ PRN04, SV34, Block IIA, EI:82, Pdi:390s
- PRN05, SV50, Block IIR-M, EI:87, Pdi:390s
- ◇ PRN06, SV36, Block IIA, EI:58, Pdi:450s
- ▲ PRN07, SV48, Block IIR-M, EI:88, Pdi:1000s
- ▼ PRN08, SV38, Block IIA, EI:77, Pdi:1000s
- ▽ PRN09, SV39, Block IIA, EI:53, Pdi:600s
- △ PRN10, SV40, Block IIA, EI:68, Pdi:480s
- ★ PRN11, SV46, Block IIR, EI:57, Pdi:730s
- ◆ PRN12, SV58, Block IIR-M, EI:49, Pdi:300s
- ⊕ PRN13, SV43, Block IIR, EI:64, Pdi:440s
- PRN14, SV41, Block IIR, EI:68, Pdi:1150s
- ◇ PRN15, SV55, Block IIR-M, EI:79, Pdi:1510s
- ◇ PRN16, SV56, Block IIR, EI:88, Pdi:650s
- ◇ PRN17, SV53, Block IIR-M, EI:69, Pdi:980s
- PRN18, SV54, Block IIR, EI:76, Pdi:750s
- ◇ PRN19, SV59, Block IIR, EI:71, Pdi:780s
- △ PRN20, SV51, Block IIR, EI:41, Pdi:850s
- ▽ PRN21, SV45, Block IIR, EI:79, Pdi:1560s
- ▽ PRN22, SV47, Block IIR, EI:88, Pdi:1270s
- △ PRN23, SV60, Block IIR, EI:75, Pdi:450s
- ★ PRN24, SV65, Block IIF, EI:53, Pdi:780s
- ★ PRN25, SV62, Block IIF, EI:44, Pdi:400s
- ⊕ PRN26, SV26, Block IIA, EI:57, Pdi:610s
- ◆ PRN28, SV44, Block IIR, EI:80, Pdi:500s
- ◆ PRN29, SV57, Block IIR-M, EI:64, Pdi:1210s
- ◆ PRN30, SV35, Block IIA, EI:84, Pdi:1290s
- PRN31, SV52, Block IIR-M, EI:77, Pdi:450s
- ◇ PRN32, SV23, Block IIA, EI:60, Pdi:720s

cm-level errors for differential GPS users using dissimilar receivers

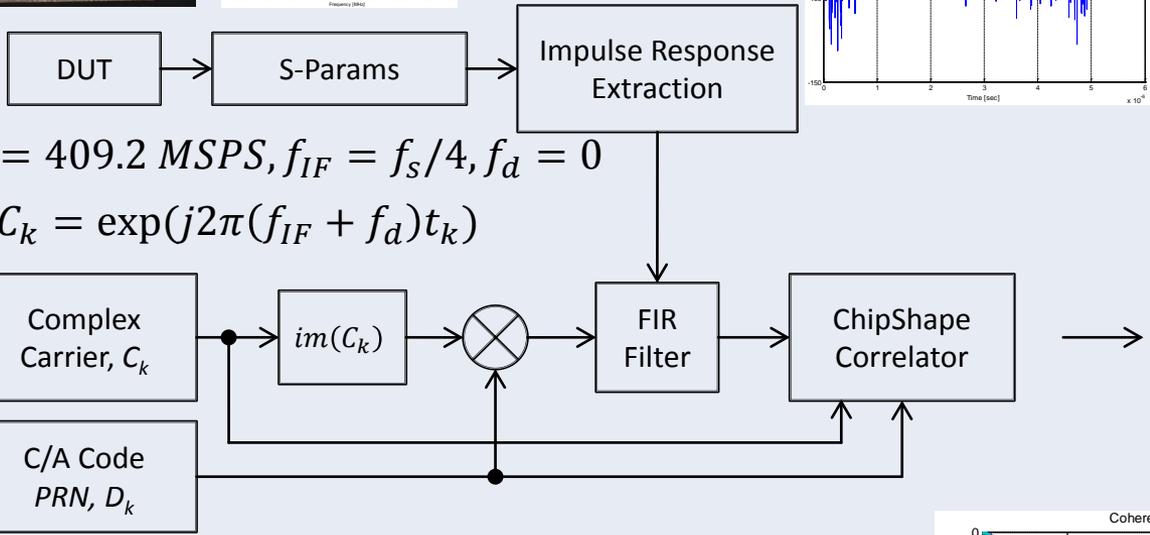
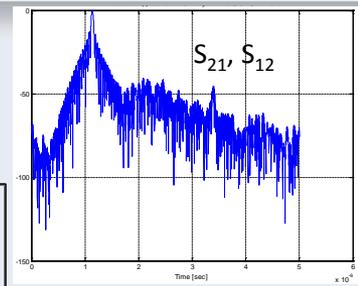
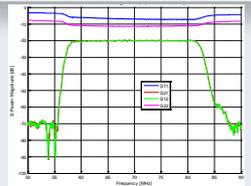
TriQuint SAWTEK 854672, f_c : 70 MHz, BW_{3dB} : 24 MHz



6x Mini-Circuits SBP 70+, f_c : 70 MHz, BW_{3dB} : 18 MHz



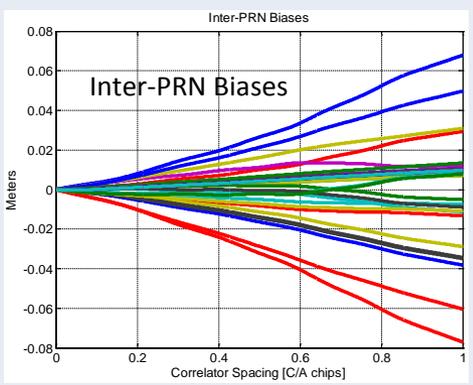
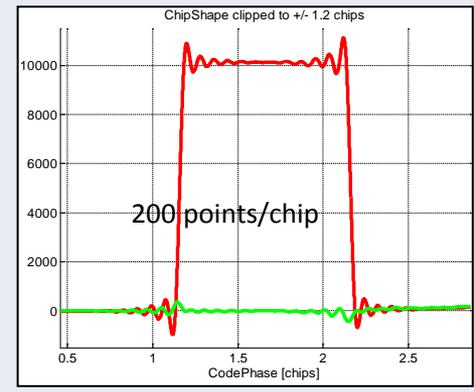
Component Effects: Processing Overview



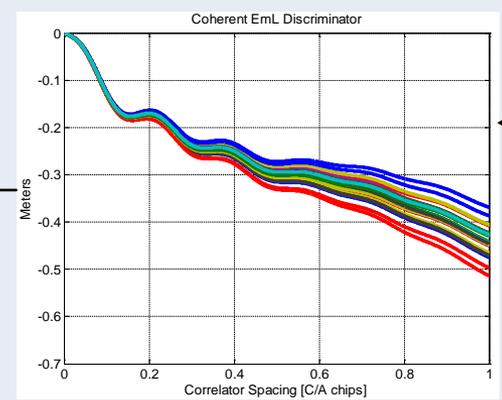
$$f_s = 409.2 \text{ MSPS}, f_{IF} = f_s/4, f_d = 0$$

$$C_k = \exp(j2\pi(f_{IF} + f_d)t_k)$$

Phase-Rotated ChipShape Function



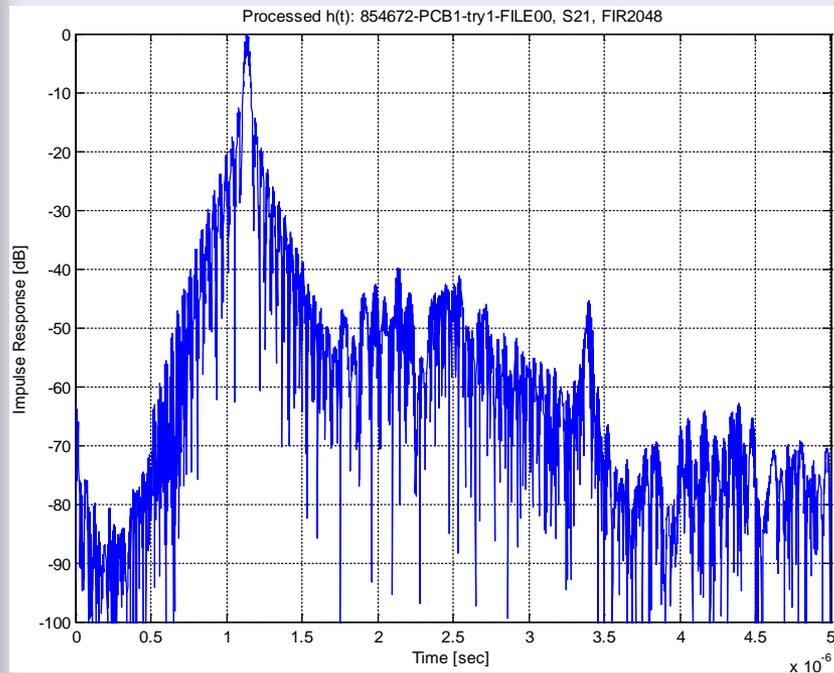
Remove Mean Response



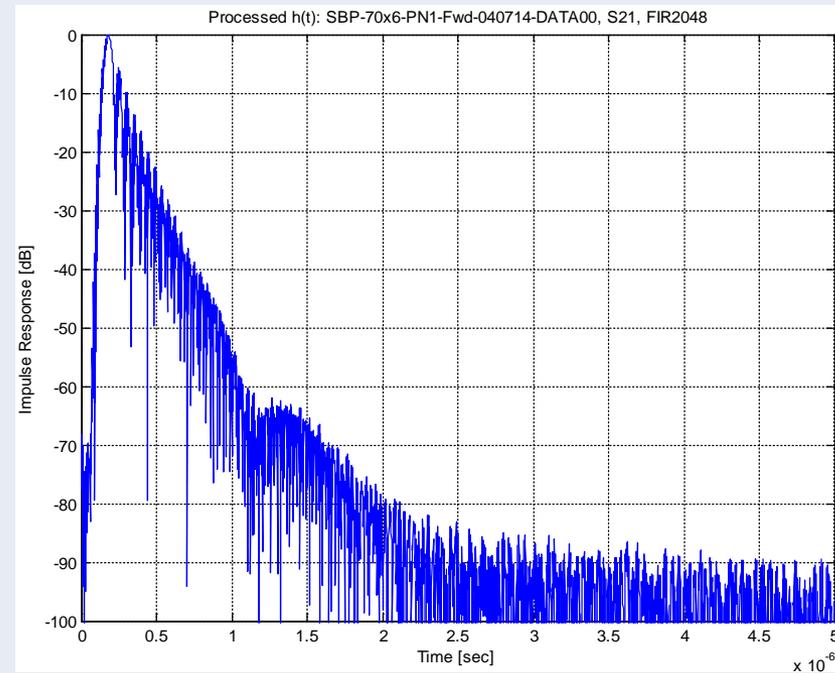
Compute Discriminator Function

$$D(d) = 0.25 \cdot c \cdot T_c \frac{R(d/2) - R(-d/2)}{R(0)}$$

Transversal SAW

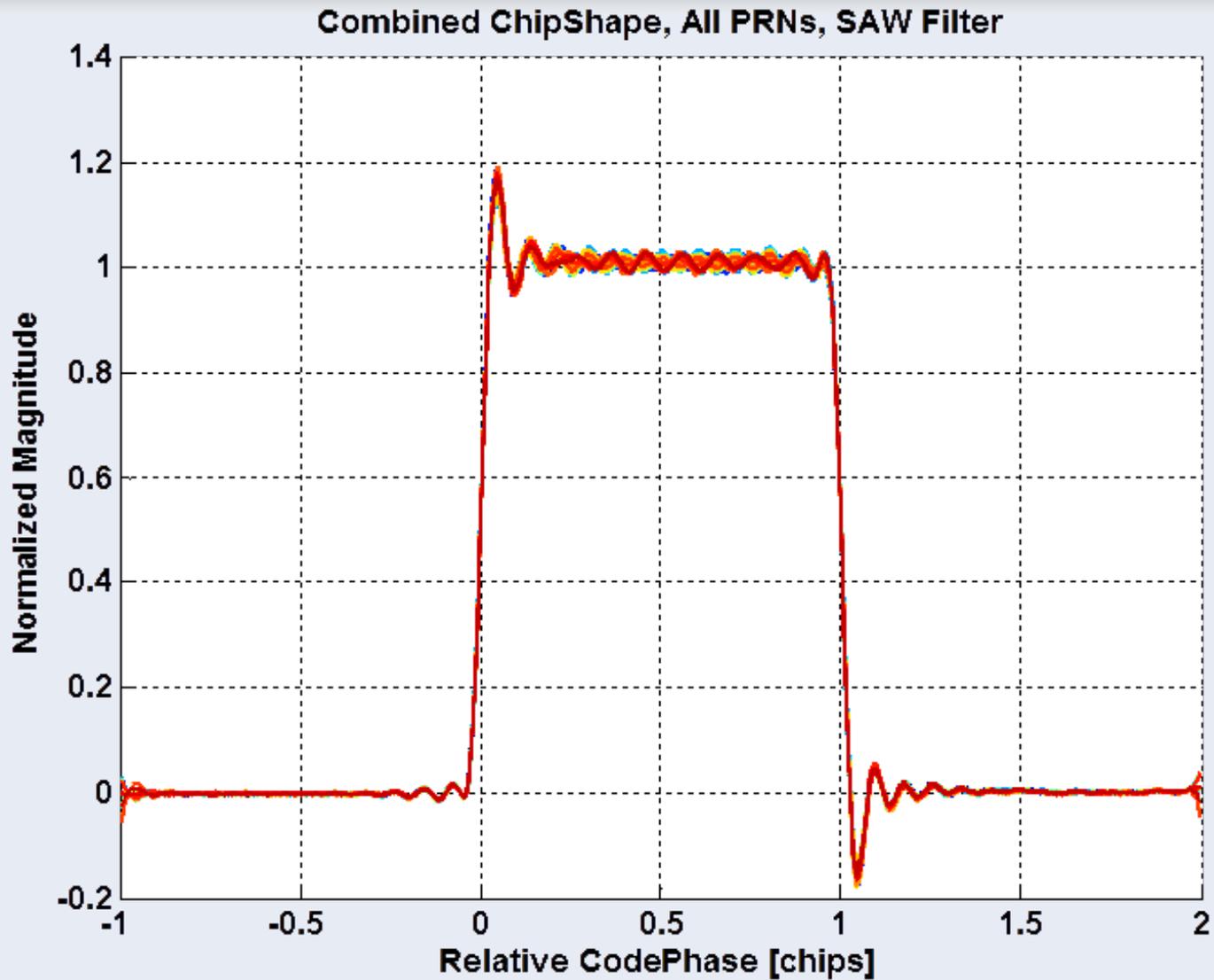


LC Elliptic Response



$R'(\tau)$ for SAW and LC Filters

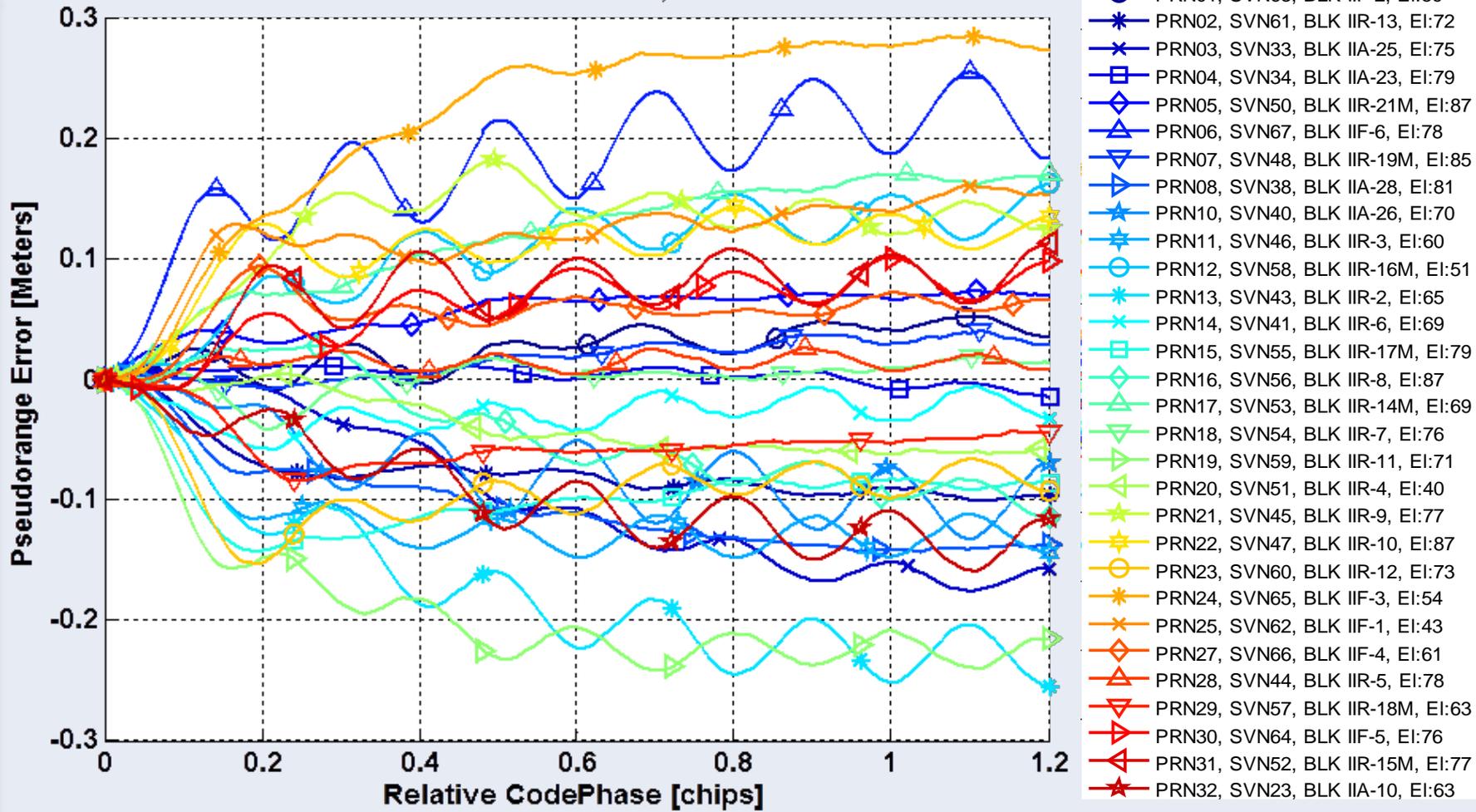
for all PRNs, $T_{pdi} = 600 \text{ sec}$



GPS-SPS Natural Biases

w.r.t. $d=0.002$, $T_{pdi} = 600 \text{ sec}$

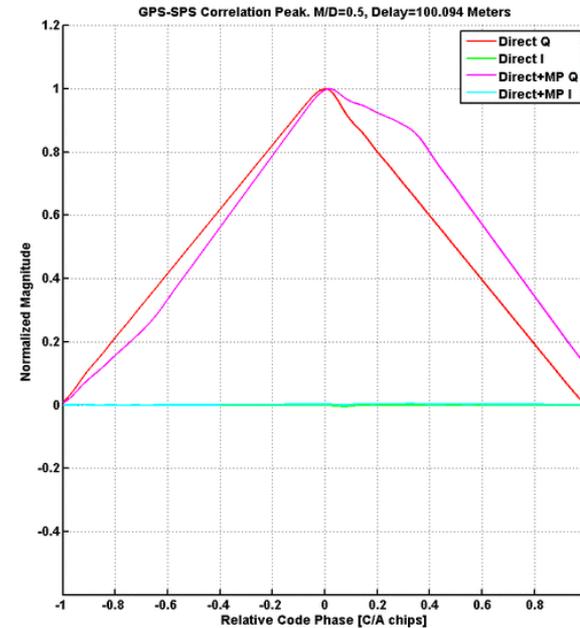
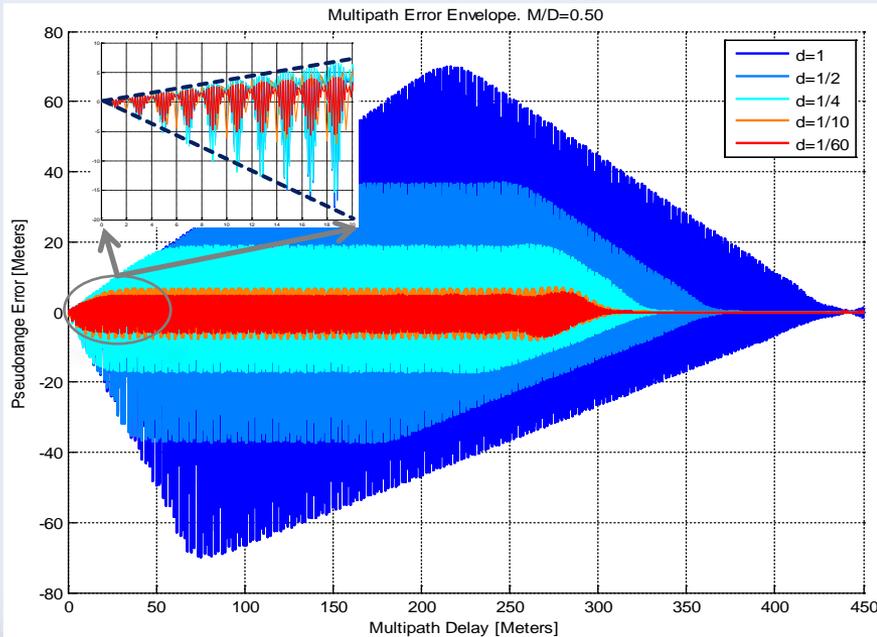
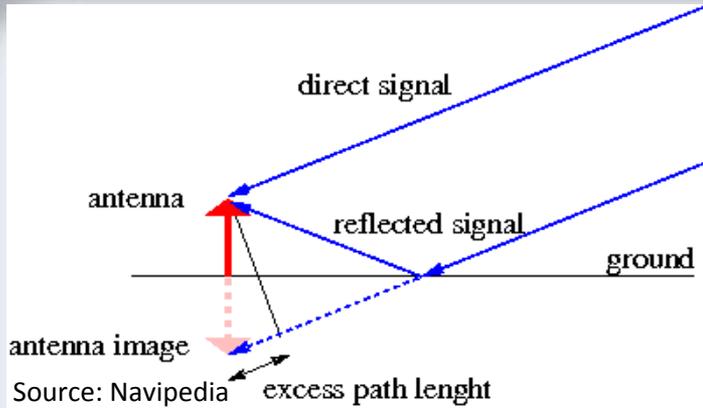
GPS-SPS Natural Biases, SAW Filter



Gunawardena & Van Graas, "GPS-SPS Inter-PRN Pseudorange Biases Compared for Transversal SAW and LC Filters Using Live Sky Data and ChipShape Software Receiver Processing," *ION ITM 2015*

measured device-to-device GPS-SPS pseudorange variation and inter-PRN biases for various filter types used in GNSS receivers

Filter: 3 dB BW & Type	#Devices Tested	Device-device variation [cm]		Inter-PRN bias [cm]	
		corr. spacing->	0.1	0.3	0.1
24 MHz L1 6-pole Cavity	1			<0.12	<0.12
20 MHz L1 3-pole Ceramic	2	<1.0	<5.0	<0.12	<0.12
40 MHz L1 BAW	2	< 20	< 70	<0.06	<0.12
24 MHz IF SAW	3	< 20	< 30	< 4.0	< 8.0
20 MHz IF SAW	5	< 12	< 30	< 1.5	< 3.0
16 MHz IF LC	2	<10	<20	<0.20	<0.30



- Narrowing correlator spacing reduces the effect of correlation peak distortion due to multipath
- Also reduces code measurement error since thermal noise on E and L become correlated (but reduces code tracking threshold)
- To reduce E-L spacing, need sufficient bandwidth to prevent top-rounding of correlation function
- More advanced techniques in use: MEDLL MET, PAC™, Strobe™ Enhanced Strobe™, double-delta
- Mitigating short-delay multipath (<15m) is still challenging

- 'Wide' 1 chip Early-minus-Late
- 1992: 'Narrow' 0.1 chip Early-minus-Late
- 1994: Multipath Eliminating Technology (MET™)
- 1999: Pulsed Aperture Correlator (PAC™) (double-delta)

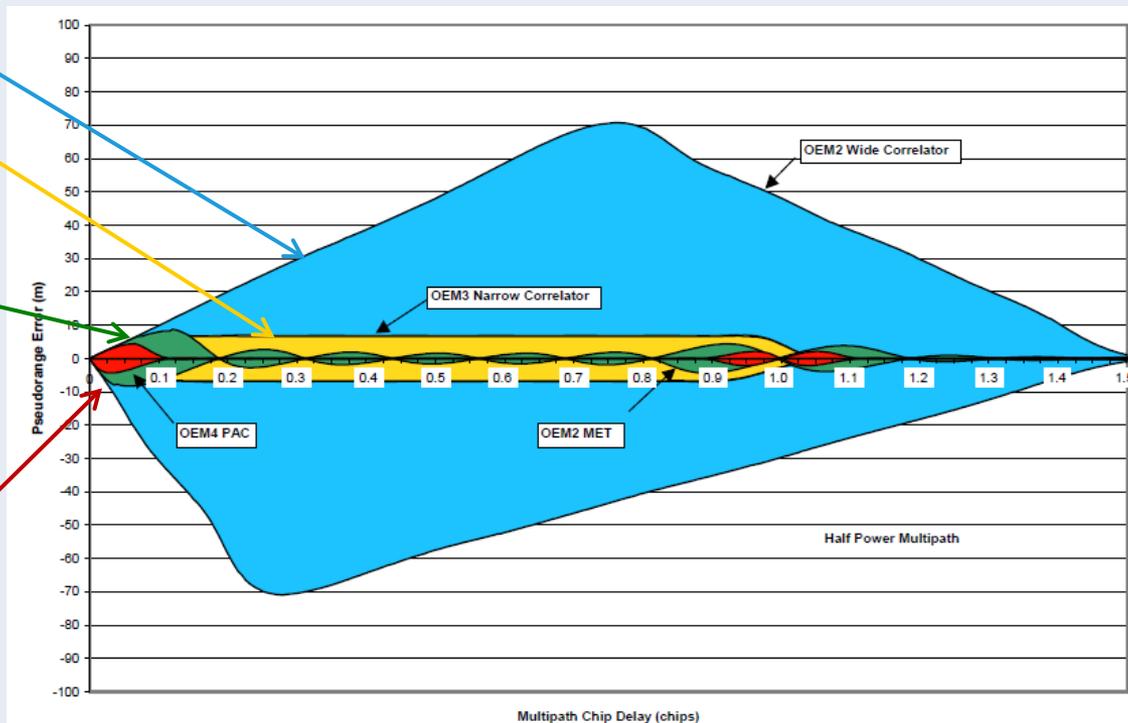
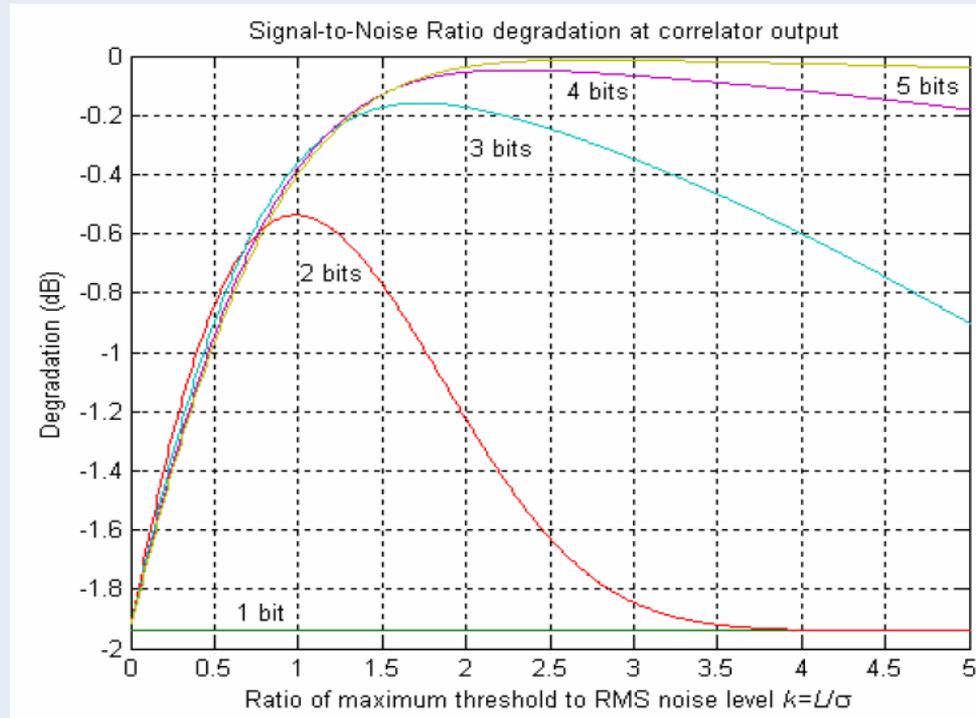


Figure 12: Comparison of multipath error envelopes

Jones, Fenton & Smith, "Theory and Performance of the Pulse Aperture Correlator"
<http://www.novatel.com/assets/Documents/Papers/PAC.pdf>

ADC Quantization Losses: S/N_0 degradation at correlator output in the presence of thermal noise only



Quantizer	1-bit	2-bit	3-bit	4-bit	5-bit
Optimal L/σ	N/A	0.9860	1.7310	2.2910	2.7225
Min Loss (dB)	1.96	0.5369	0.1589	0.0472	0.0138

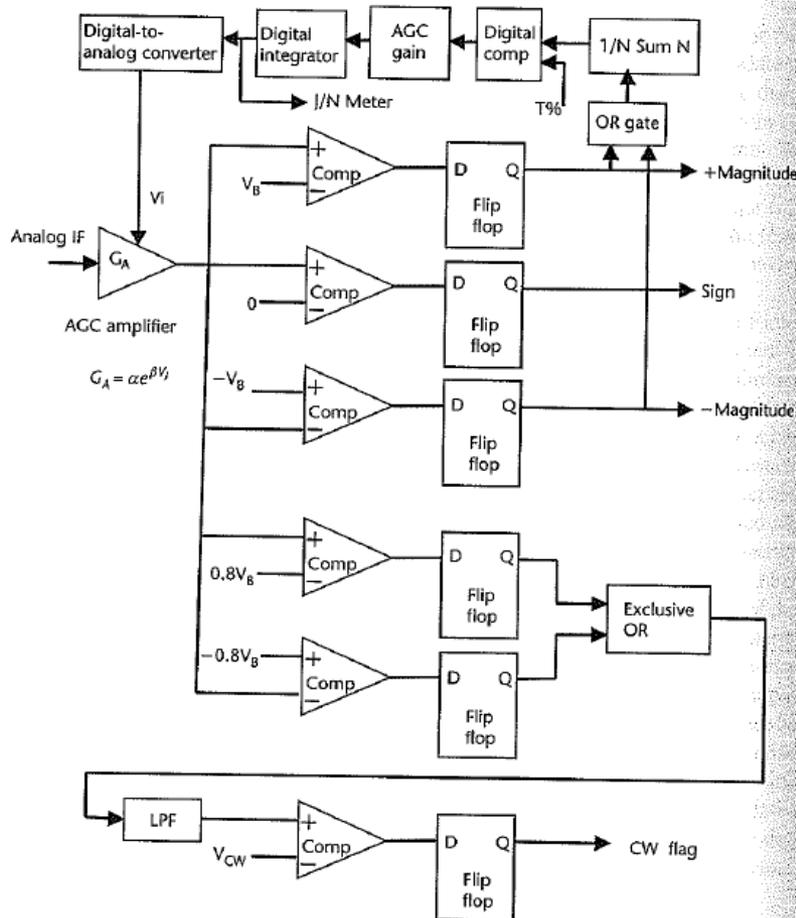


Figure 6.1 AGC amplifier followed by a nonuniform ADC, CW detector, and digital I/N meter.

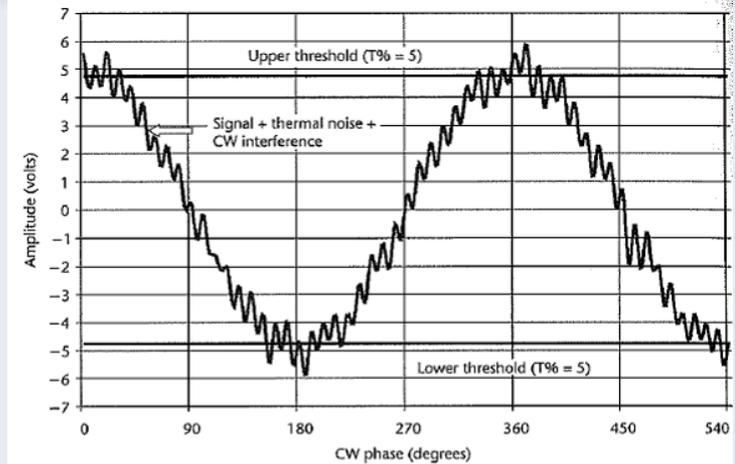
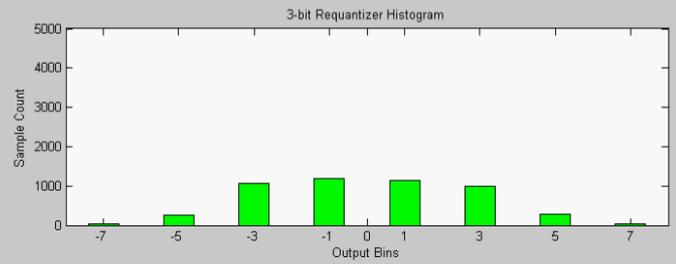
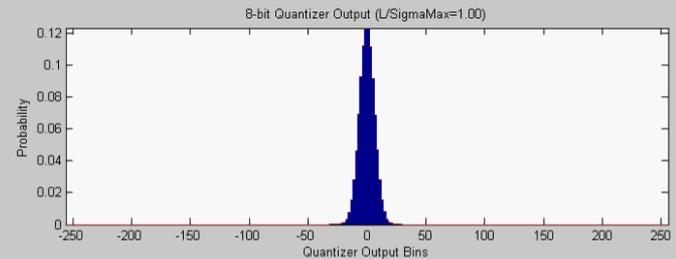


Figure 6.3 Setting nonuniform ADC threshold to exploit constant envelope interference statistics.

'Crest-Riding' Implemented on 8-bit Samples

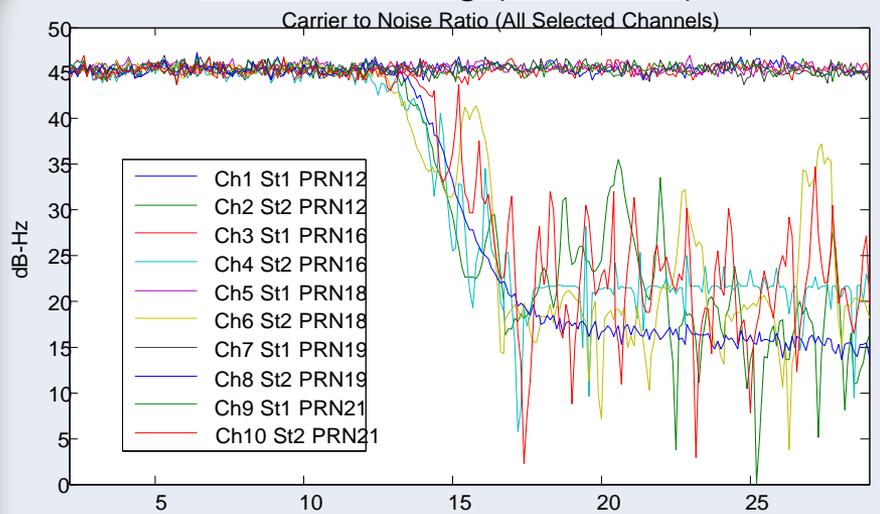


scanned images from Kaplan & Hegarty, "Understanding GPS: Principles and Applications, Second Edition," Nov. 2005

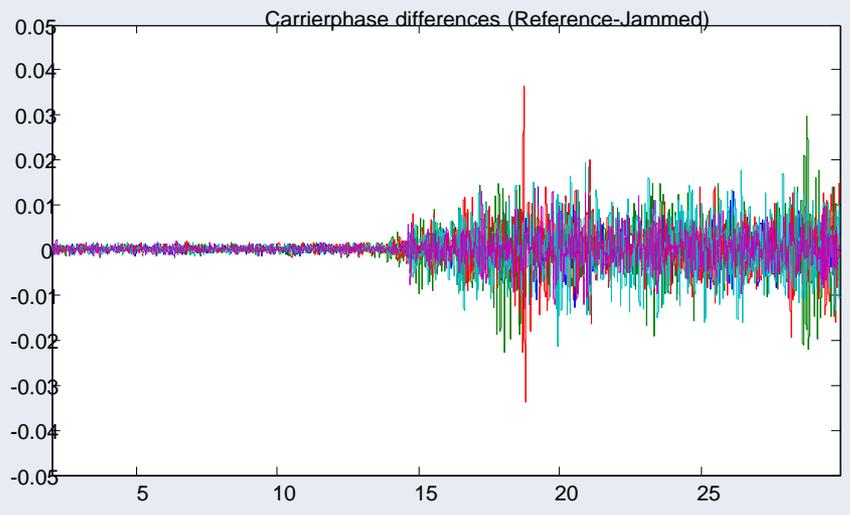
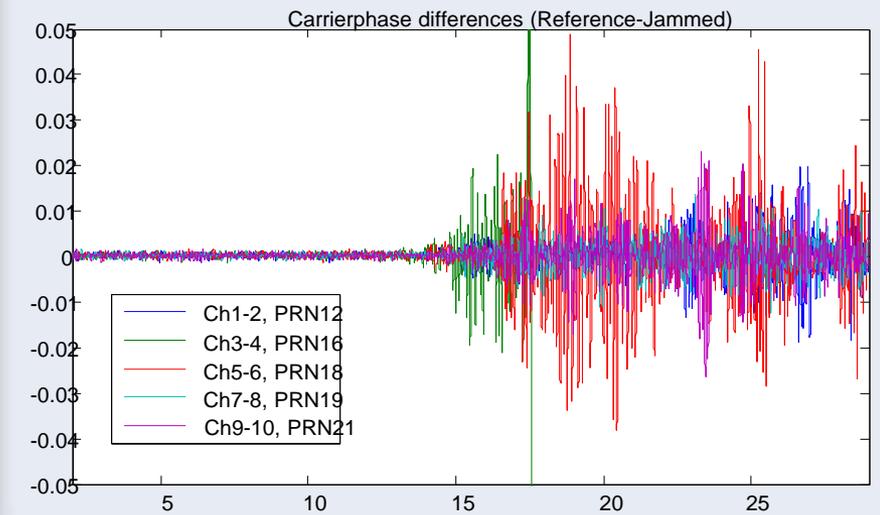
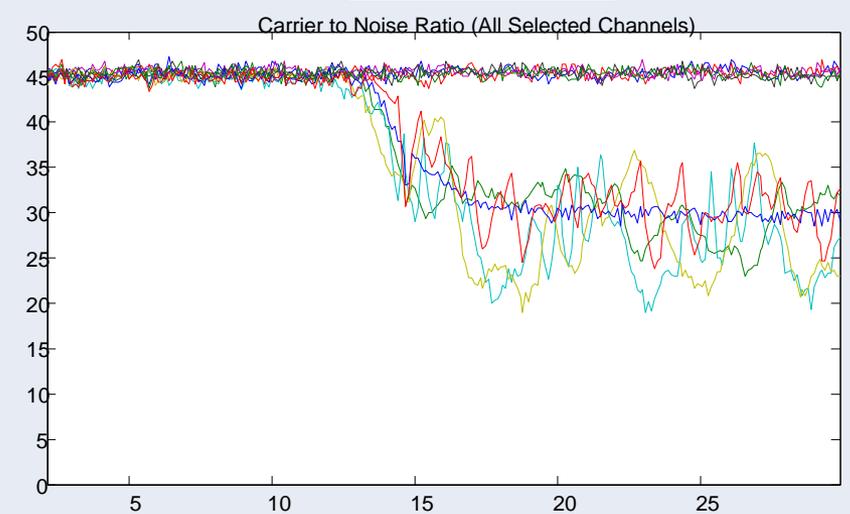
Digital 'Crest Riding' Re-Quantizer Performance

50 dB ISR Swept FM, 1MHz Span

No Processing (8-bit data)



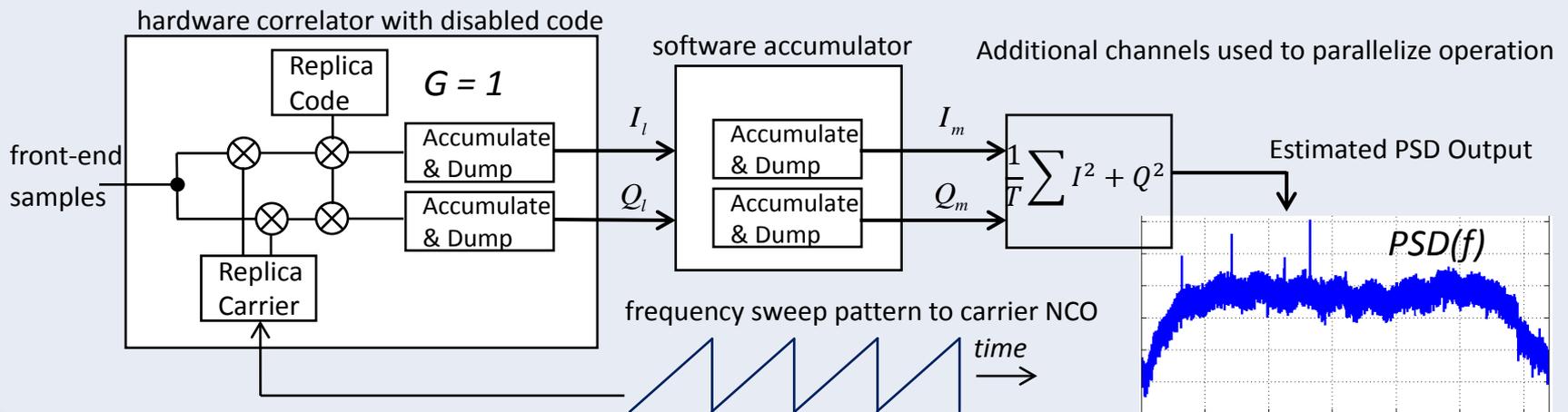
Re-Quantized



Ref: Gunawardena, et al, Multi-Channel Wideband GPS Anomalous Event Monitor, ION GNSS 2011

Technique	Pros	Cons
AGC voltage monitoring as an indicator of in-band interference	<ul style="list-style-type: none"> Free indicator (already exists in most receiver front-ends) Can be used to activate other situational awareness indicators 	AGC voltage changes due to temperature variations and antenna orientation → false alarms
Dedicated sample variance and FFT processing blocks	Dedicated/direct estimators of in-band power and spectrum for reporting GNSS band quality	Requires integration into new receiver designs. Needs dedicated resources. Increased power consumption
Swept-Frequency PSD estimator using one or more existing receiver channels	Can be implemented on existing receivers (one or more spare channels). Frequency resolution adjustable via pre-detection integration time	Cannot observe 'instantaneous' spectrum; may misrepresent pulsed interference; consumes receiver channels

Low-Cost Swept-Frequency Spectral Situational Awareness Monitor using Spare Channel(s)



More on GPS PPP



Sunil Bisnath
Associate Professor
York University

Standard Positioning Service

m-level real-time broadcast GPS orbit and clock information

+

User GPS satellite C/A-code tracking information

+

Epoch measurement filtering

=

m-level user position estimate

Precise Point Positioning

cm-level real-time or post-processed precise GPS orbit and clock information

+

User GPS satellite L1/L2 code and phase tracking information

+

Sequential measurement filtering

+

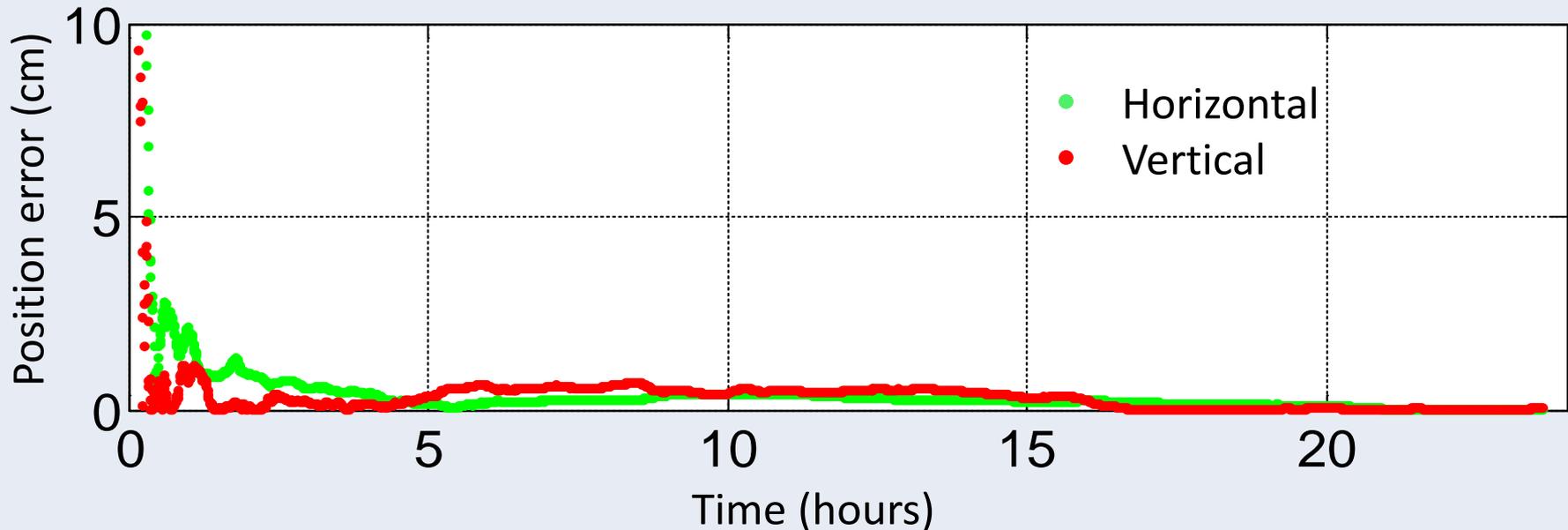
Additional error modeling

=

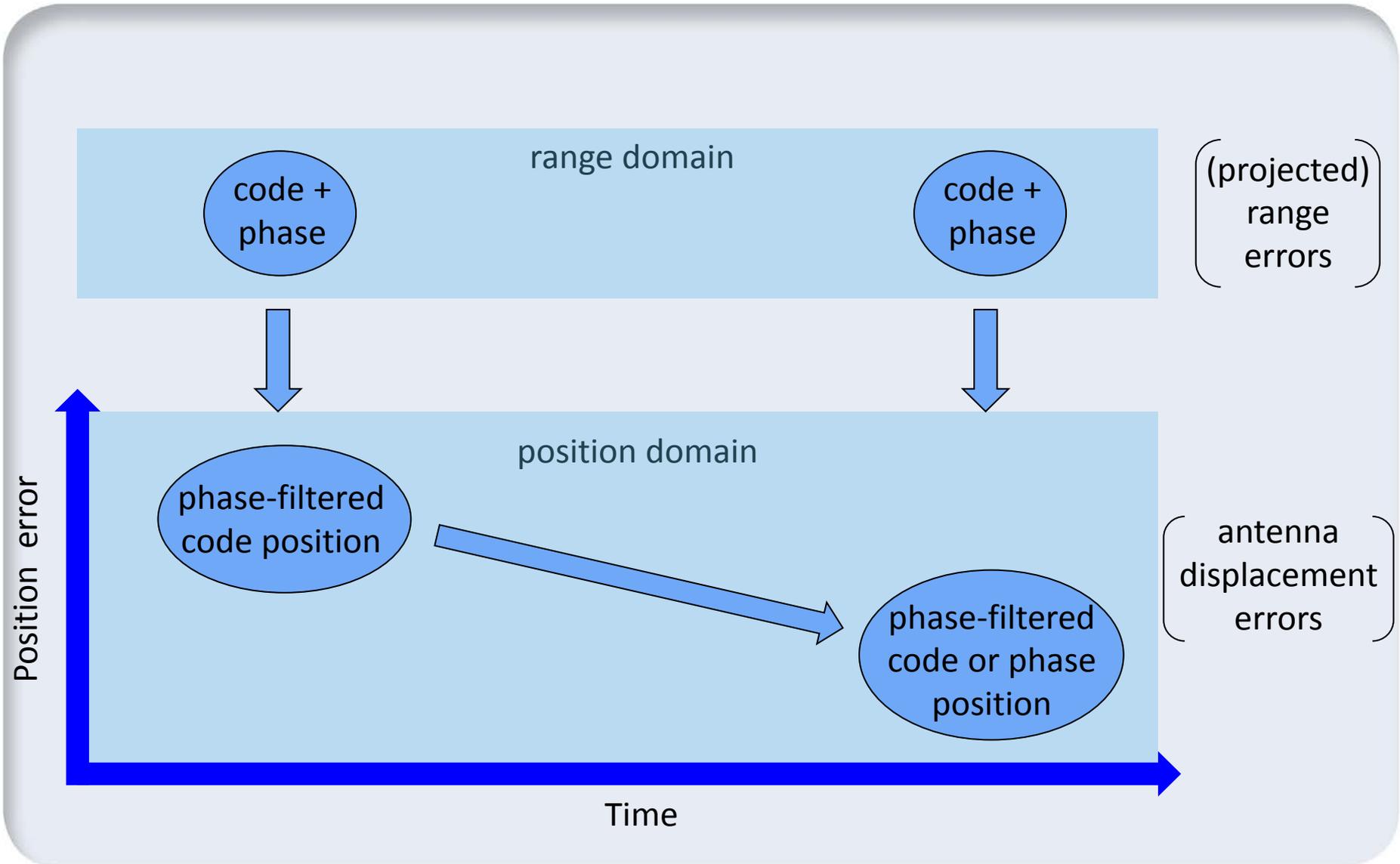
dm- to mm-level user position estimate

ASPECT	PPP	RTK / NETWORK RTK
Coverage	Global	Local / regional
Range limitation	None	Baseline / network
Positioning accuracy	dm - mm	cm - mm
User hardware	Single geodetic receiver	Single geodetic receiver
Infrastructure	Global CORS network	Single CORS / regional CORS network
Corrections	GPS orbits and clocks	Single CORS measurements / CORS measurements; orbit and atmospheric corrections
Communications	Satellite; Internet; post-processing	Radio / cellular
Major limitation	Convergence period	Range

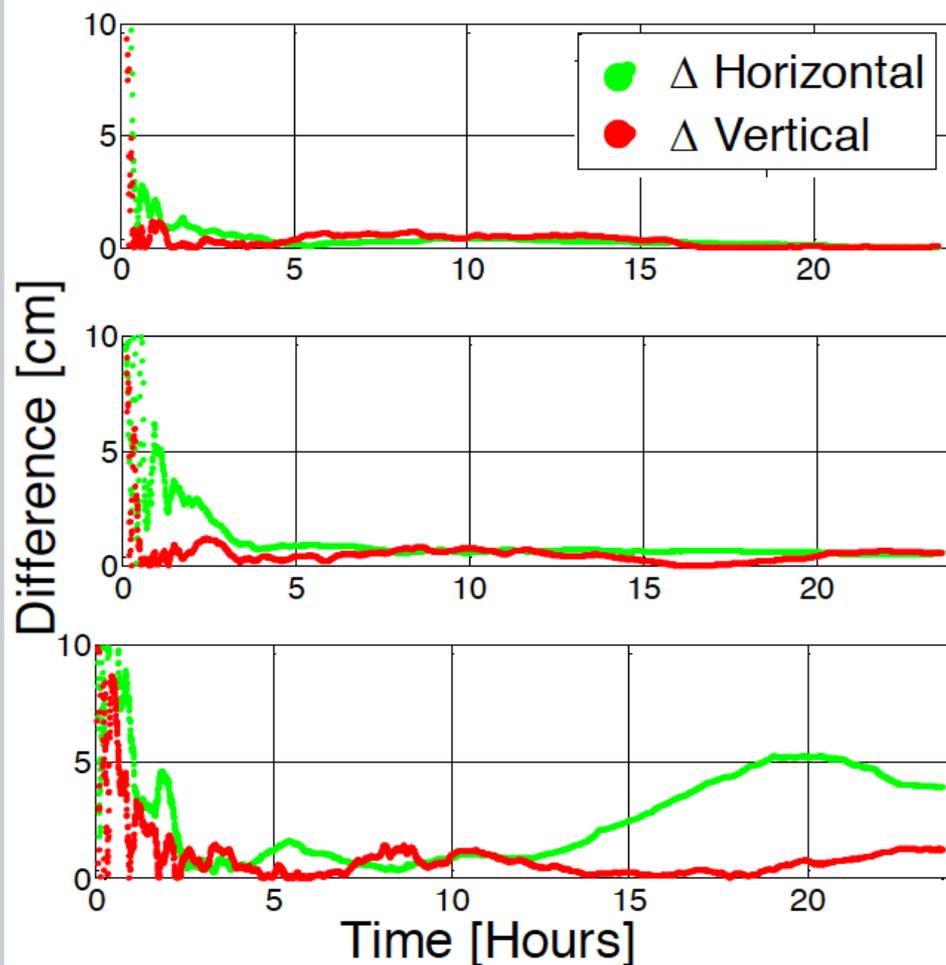
- A good, static GPS PPP positioning solution over 24 hours



- Characteristic PPP initial convergence period
- Solution very stable post-convergence
- Solution gap requires re-convergence as shown



24 hour static solutions



Site : RIGA, RIGA Above average convergence

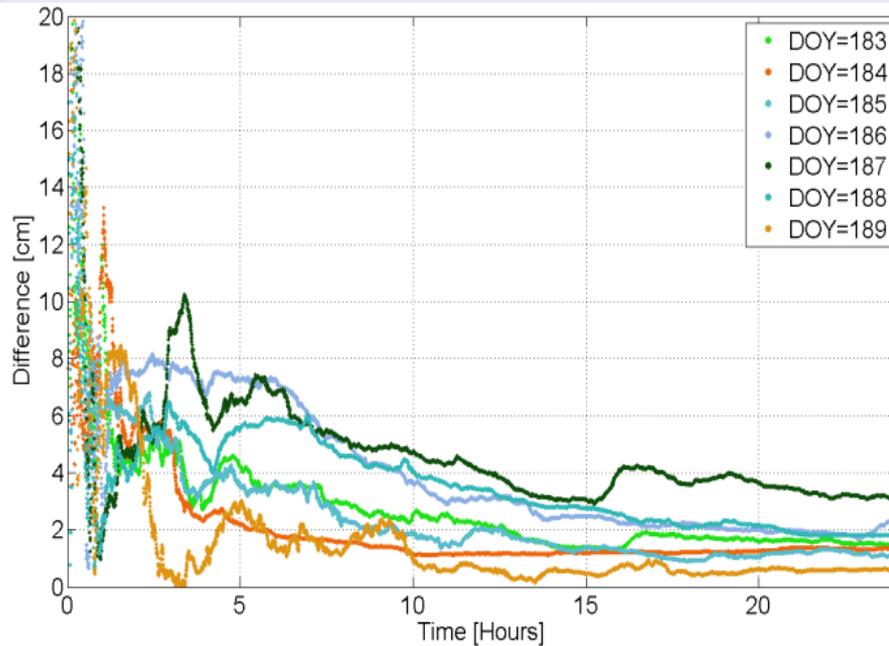
Statistic (mm)	2D	Up	3D
Bias	3	3	4
std dev	2	5	5
rms	4	6	7

Site : CONT, Concepcion Typical convergence

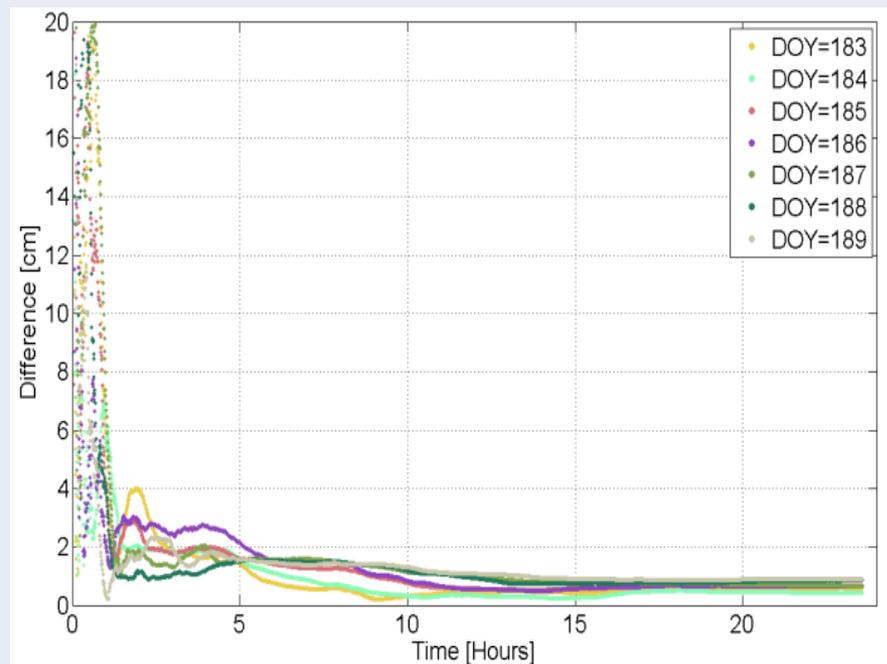
Statistic (mm)	2D	Up	3D
Bias	9	-11	14
std dev	2	2	3
rms	9	11	14

Site : POVE, Porto Velho Poor convergence

Statistic (mm)	2D	Up	3D
Bias	29	-1	29
std dev	10	10	14
rms	31	26	32

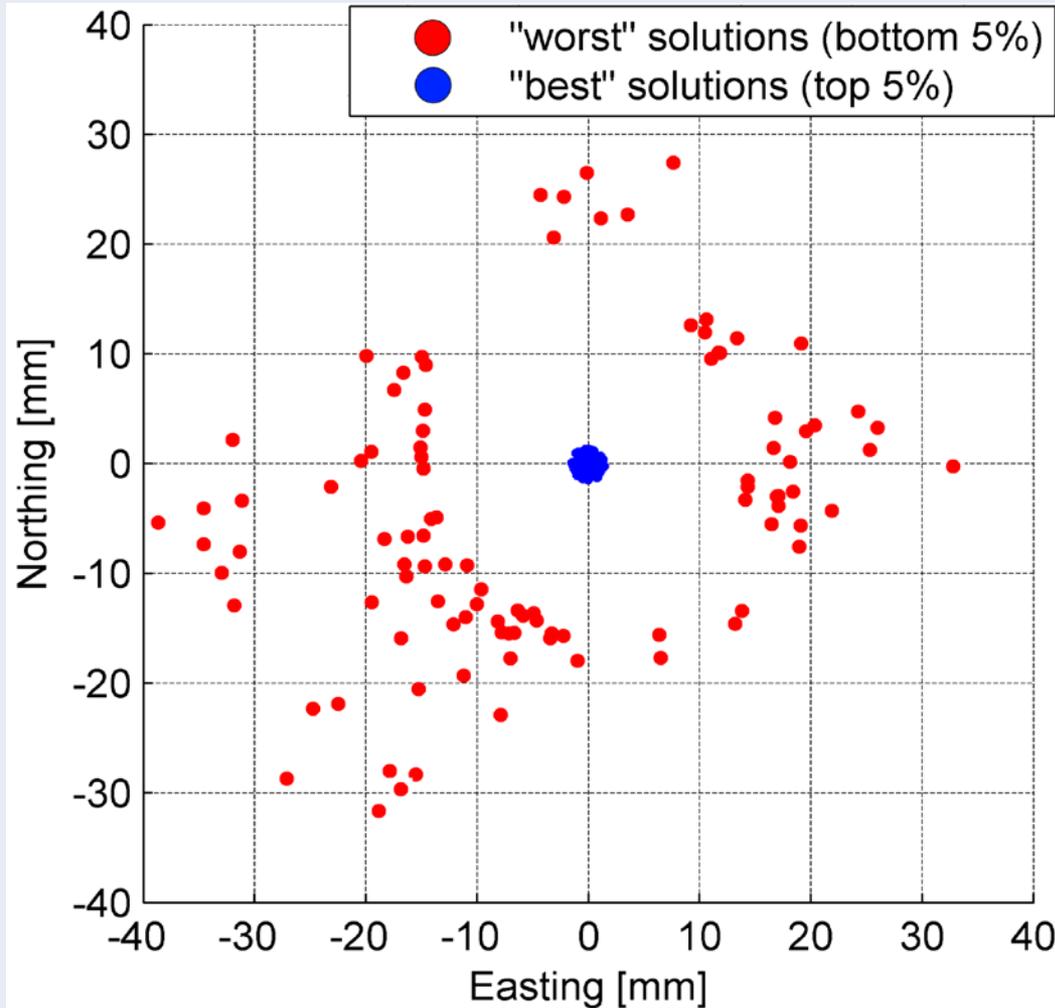


AZU1
Azusa, California



WHC1
Whitter College, California

stations < 10 km apart
(static processing)



- 1 week, 300 global IGS stations
- Daily position error
- Static processing

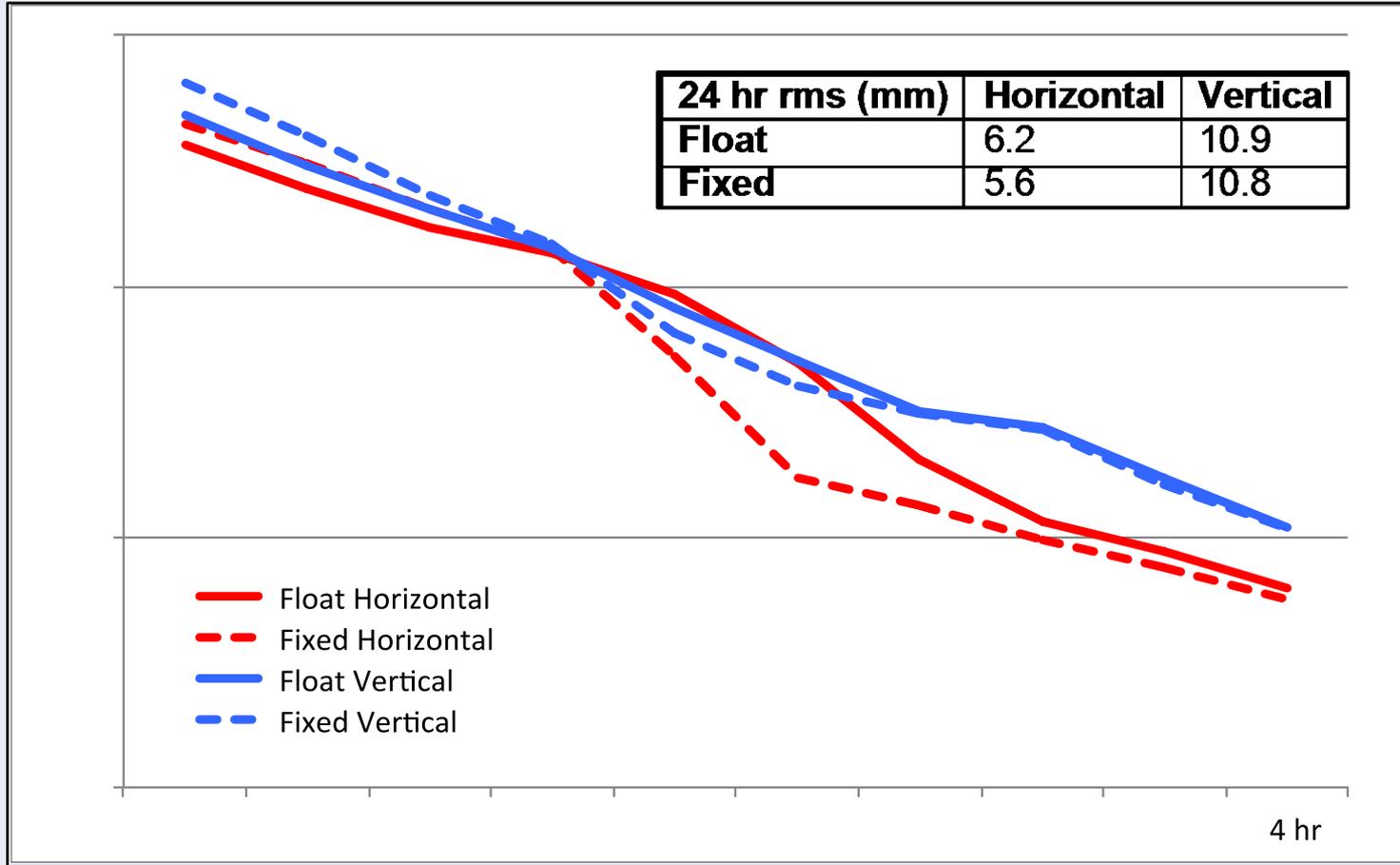
- Potential benefits of ambiguity resolution:
 - (Greatly) reduced convergence period
 - Higher positional accuracy
 - More consistent solutions
 - All resulting in more robust processing technique
- Initial attempts at fixed PPP through modeling of small satellite and receiver time mis-synchronization biases resulted in over-parameterization of model:

$$P_3 = \rho + T + c(dt^r - dt^s) + b_{P3}^r - b_{P3}^s + \varepsilon_{P3}$$

$$L_3 = \rho + T + c(dt^r - dt^s) + b_{L3}^r - b_{L3}^s - \lambda_3 N_3 + \varepsilon_{L3}$$

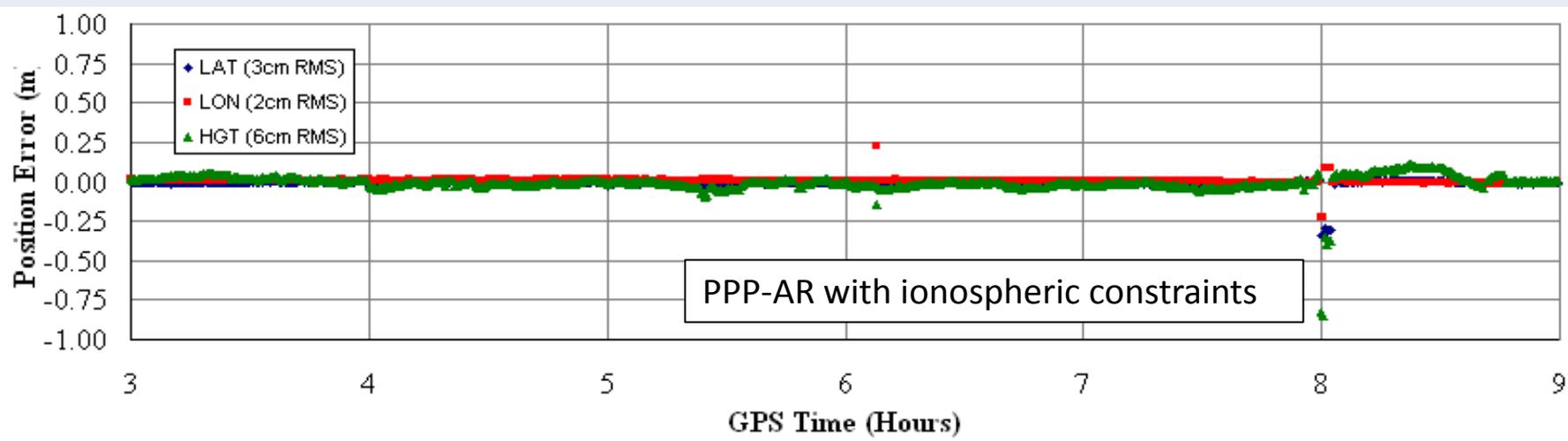
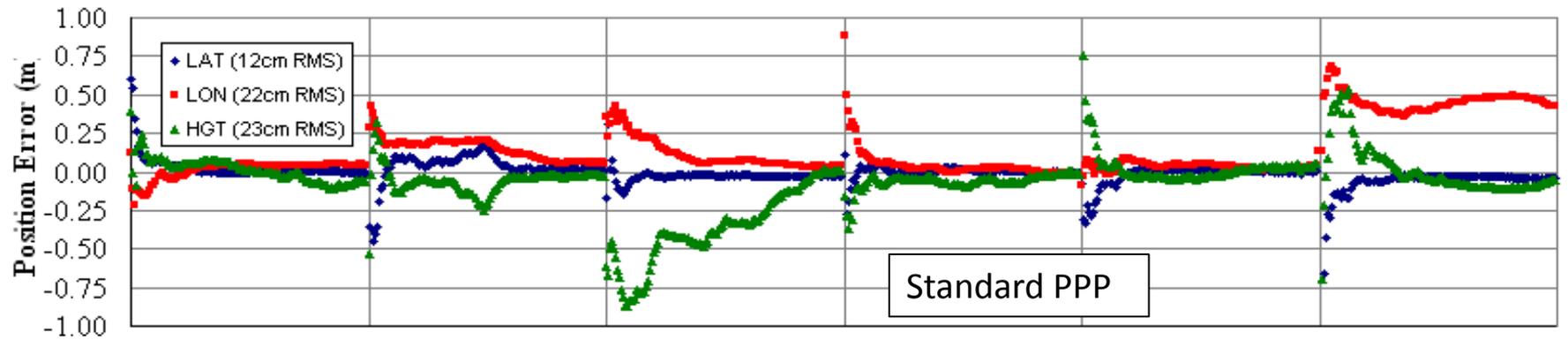
- *So question is: How to resolved PPP ambiguities – with no or limited assumptions about timing biases?*

- A few methods nominally equivalent approaches have been developed to resolve PPP ambiguities, e.g.:
 - Decoupled clocks (NRCan)
 - Integer clocks (CNES)
 - Uncalibrated hardware delays (GFZ / Wuhan / Nottingham)
- ‘Decoupled clock model’ and ‘Integer clocks’ re-parameterize observation equations to isolate code biases from ambiguity estimates
 - (In principle) permits ambiguity resolution
 - Phase ambiguity moved to phase clock parameters
 - Ionosphere-free wavelength amplified with widelane
- ‘Uncalibrated hardware delays’ computes offsets relative to IGS clocks to access integer ambiguities via single difference
- All require additional satellite bias products for users, computed from global network solution



- Instead of ionospheric-free code and phase, use undifferenced four observables
- Ionospheric parameter is corrupted by biases
- Carry-out implicit differencing to estimate relative ionosphere
- Same way ambiguities are differenced in decoupled clock model to isolate their relative integer character

- Ionosphere parameter can provide constraint on ambiguity resolution when, e.g., loss of lock, data gap, etc. is experienced
- When all ambiguities are reset, should provide rapid *re-convergence* of solution



Ask the Experts – Part 1



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M.Sc, M.E., P.Eng.
Manager
Applied Technology Group
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Poll #2

Performance wise (accuracy, integrity) which one do you think is true?

- GPS + GLONASS PPP is equivalent to GPS-only PPP.
- GPS + GLONASS PPP is better than GPS-only PPP.
- GPS + GLONASS PPP is worse than GPS-only PPP.
- It is not that simple.

High Accuracy GNSS

Disclaimers:

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Components, equipment and manufacturers discussed are for information purposes only. The author does not endorse any manufacturers, products, services, or the suitability of any products referenced herein for any particular purpose

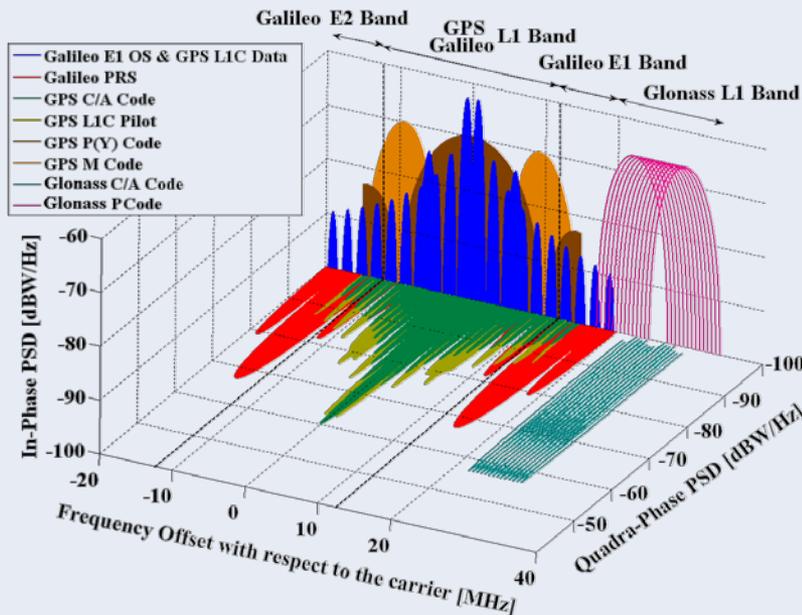


Sanjeev Gunawardena
Research Assistant Professor
Air Force Institute of Technology

GLONASS Signals on L1

1598.0625 – 1604.2500 MHz

- Contains standard precision (SP) and high precision (HP) services using FDMA modulation
- L1 center frequency for channel k : $f_c = 1602 + k \times 0.5625$ [MHz] where $k = -7, -6, \dots, 4$ (1598.0625 – 1604.2500)
- P Code: $R_c = 5.11$ Mcps, 33,554,432 chips long, 25-bit LFSR, repeats every second [Kaplan & Hegarty].
- Receiver inter-channel biases due to FDMA represents challenge for receiver designers
- Front-end group delay for each channel must be determined and measurements calibrated accordingly



GNSS System	GLONASS	GLONASS
Service Name	C/A Code	P Code
Centre Frequency	(1598.0625-1605.375) MHz \pm 0.511 MHz	
Frequency Band	L1	L1
Access Technique	FDMA	FDMA
Spreading modulation	BPSK(0.511)	BPSK(5.11)
Sub-carrier frequency	-	-
Code frequency	0.511 MHz	5.11 MHz
Signal Component	Data	Data
Primary PRN Code length	511	N/A
Code Family	M-sequences	N/A
Meander sequence	100 Hz	N/A
Data rate	50 bps	N/A
Minimum Received Power [dBW]	-161 dBW	N/A
Elevation	5°	N/A

Source:

www.navipedia.net/index.php/GLONASS_Signal_Plan

Relevant public ICD:

- ICD L1, L2 (ed. 5.1 2008)

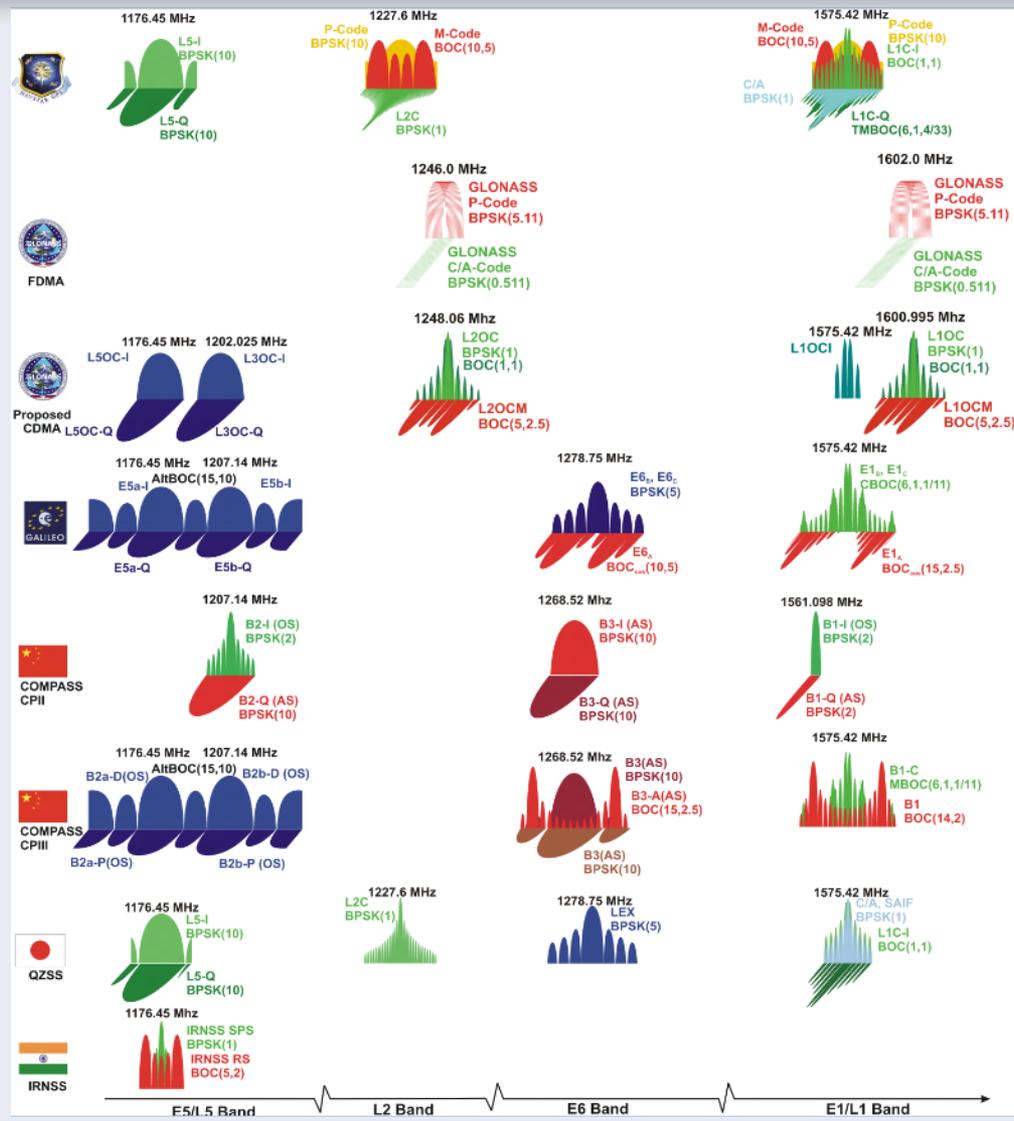
Also read: U. Roßbach, [Positioning and Navigation Using the Russian Satellite System GLONASS, 2001](#)

Increasing cost and complexity



Technique	Pros	Cons
One-time factory calibration of nominal biases	Simple, supports mass production	Not sufficient for high-accuracy applications
Factory calibration as a function of temperature. Store calibration values in memory	Suitable for medium-volume cost-sensitive GPS/GLONASS receivers	Requires front-end temperature sensing. Longer and more complex calibration procedure.
Integrated closed-loop calibration using built-in 'group delay meter'	Continuous dynamic estimation of inter-channel biases using group delay measurements	Works primarily for self-contained receivers (i.e. no detached antenna). High cost and complexity.

GNSS 'Spectral Landscape' Present & Future



Ref: www.navipedia.net/images/c/cf/GNSS_All_Signals.png

GNSS PPP



Sunil Bisnath
Associate Professor
York University

BENEFITS:

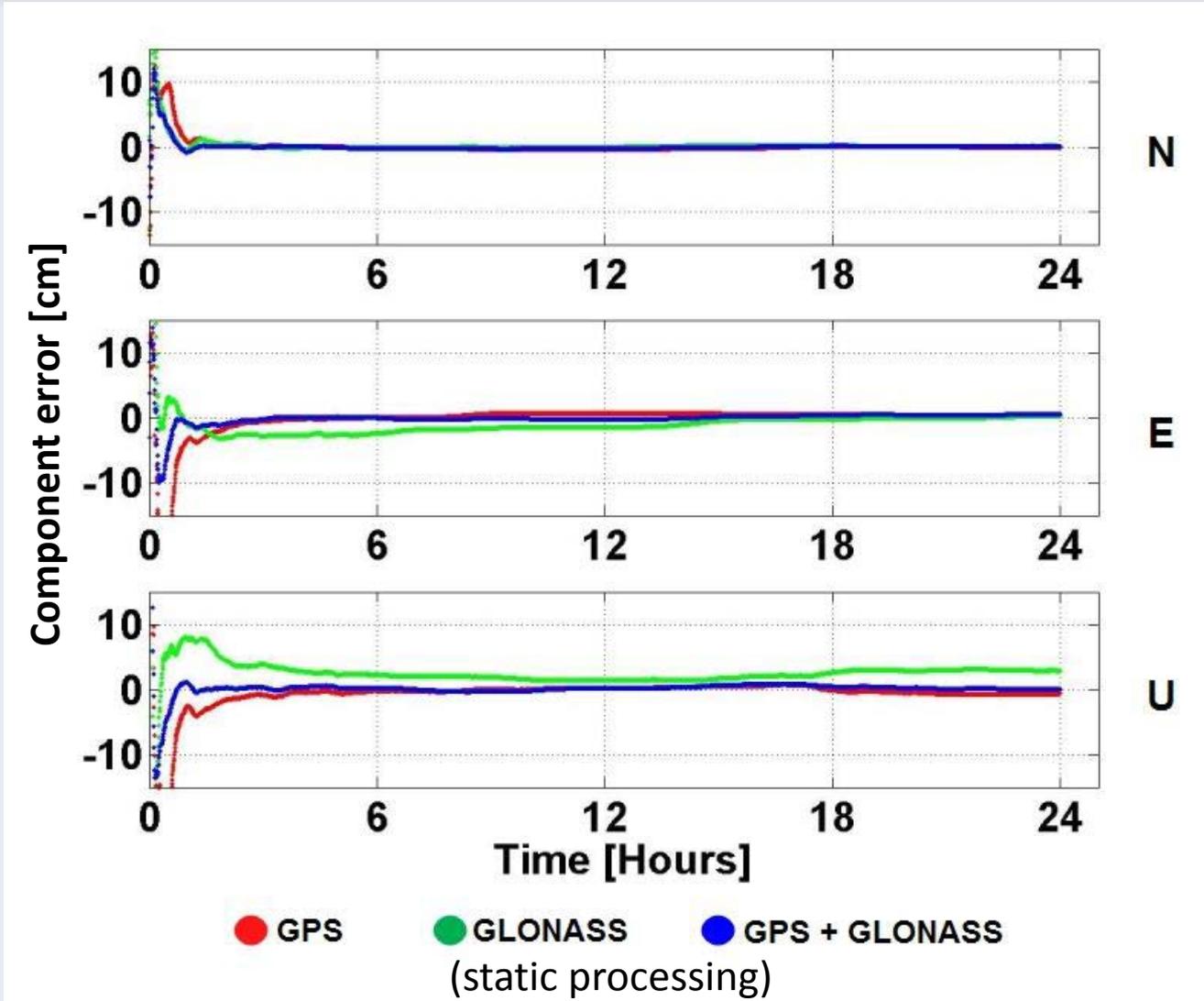
- Measurement sensitive technique →
- More measurements + varied geometry = improved positioning

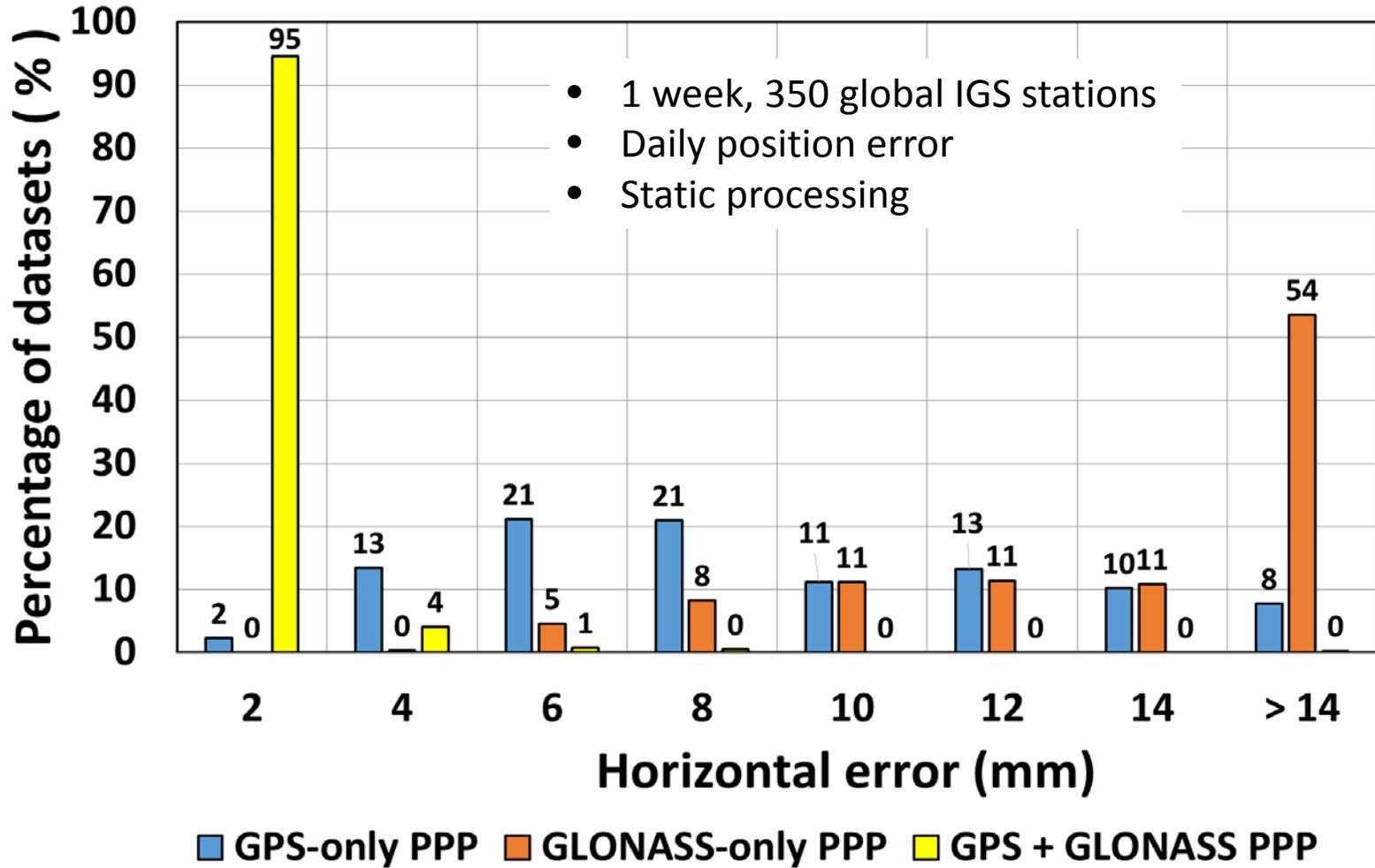
ISSUES:

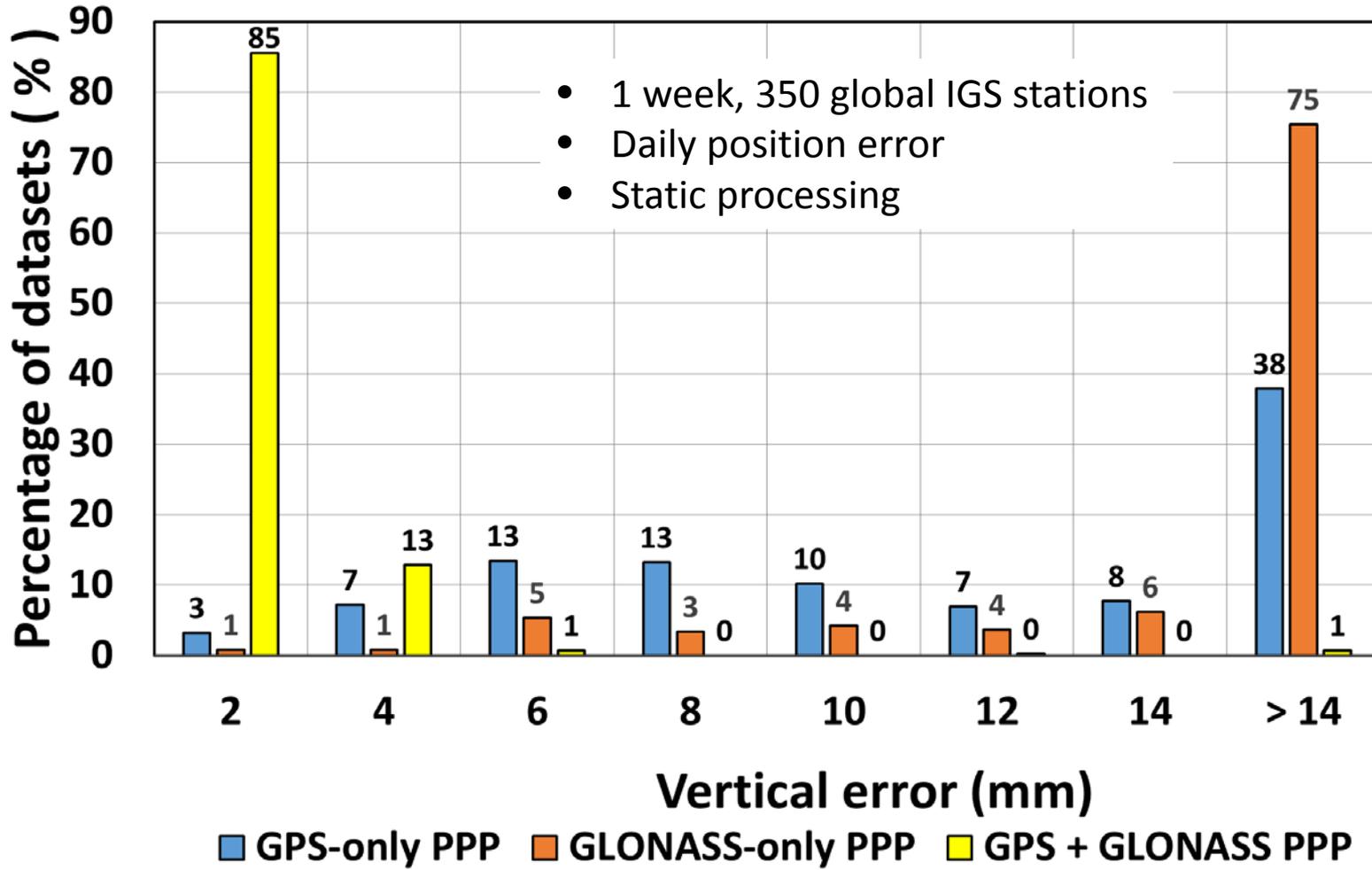
- Different spatial reference systems for different systems
- Different temporal reference systems for different systems
- GLONASS is FDMA, while all other systems are CDMA
- Managing various equipment biases within and between systems

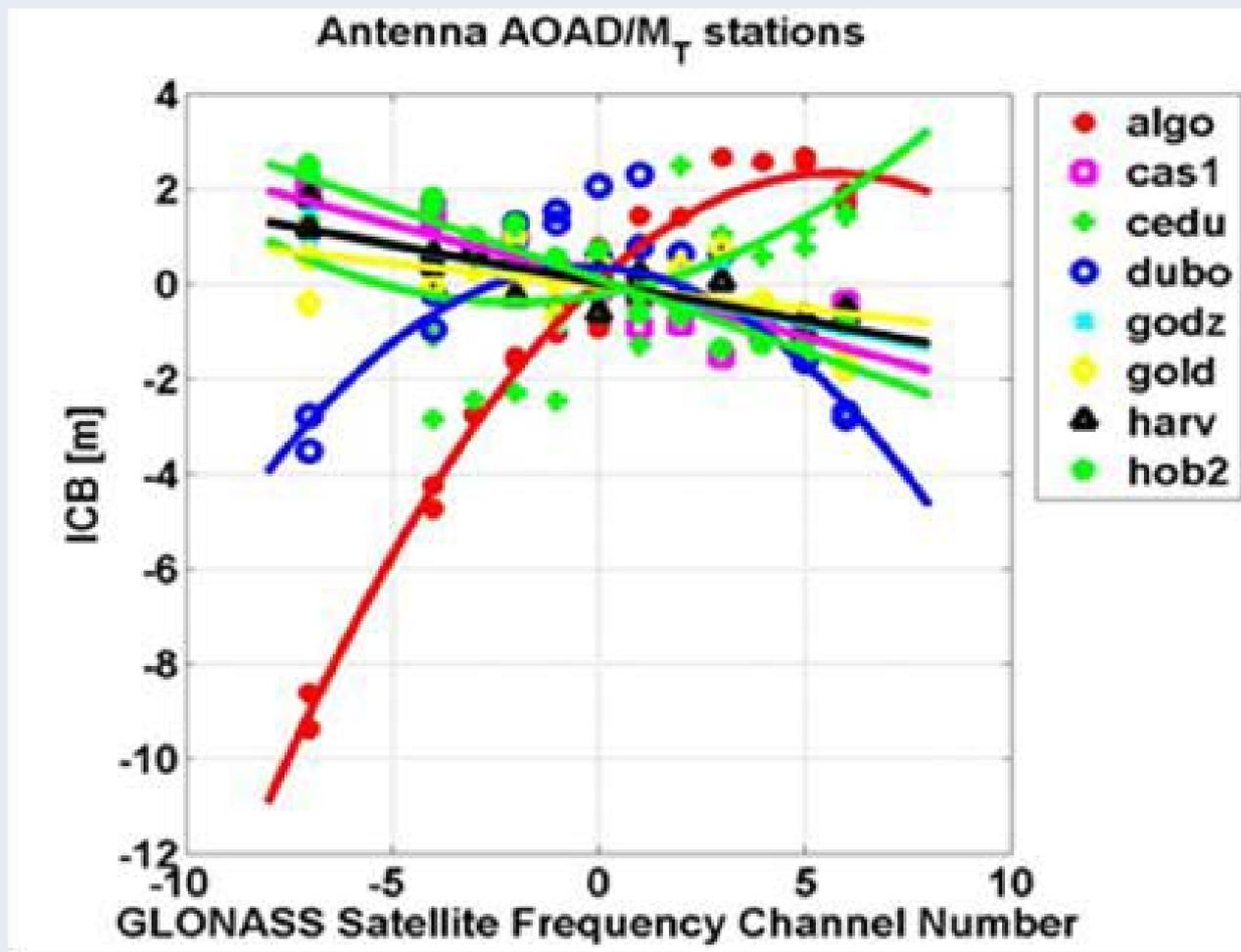
- Popular terms: “hardware biases” or “hardware delays” or “instrumental delays”, referring to errors introduced in the equipment (circuitry and electronics)
- Satellite instrumental delays and receiver instrumental delays
- Some delays estimated by tracking network
- Others modeled as an additional term added to code and phase observation equations
- Often implied modeling: added to receiver noise / SV hardware delay / multipath term

- DCB Differential Code Bias $P2-P1$
- DPB Differential Phase Bias $L2-L1$
- RCB Relative Code Bias $P1-C1, P2-C2$
- RPB Relative Phase Bias $L1(P)-L1(C), L2(P)-L2(C)$
- CPB Code-Phase Bias $C1-L1(C), P1-L1(P), \text{ etc.}$









- Pseudorange ICBs
- 8 stations
- Same antenna types
- Different receiver types and firmware versions

- **New GNSS signals enhancing PPP (and RTK) performance**
- Most network RTK services are now GPS+GLONASS
- GPS+GLONASS PPP with AR and fast re-convergence commercially available

- ***Fast RTK-like initialization for PPP is still goal***
- Integration of PPP and network RTK processing
- Early GPS+GLONASS+BEIDOU+GALILEO PPP results show further improvements
- Triple-frequency GPS PPP-AR simulations show very fast convergence



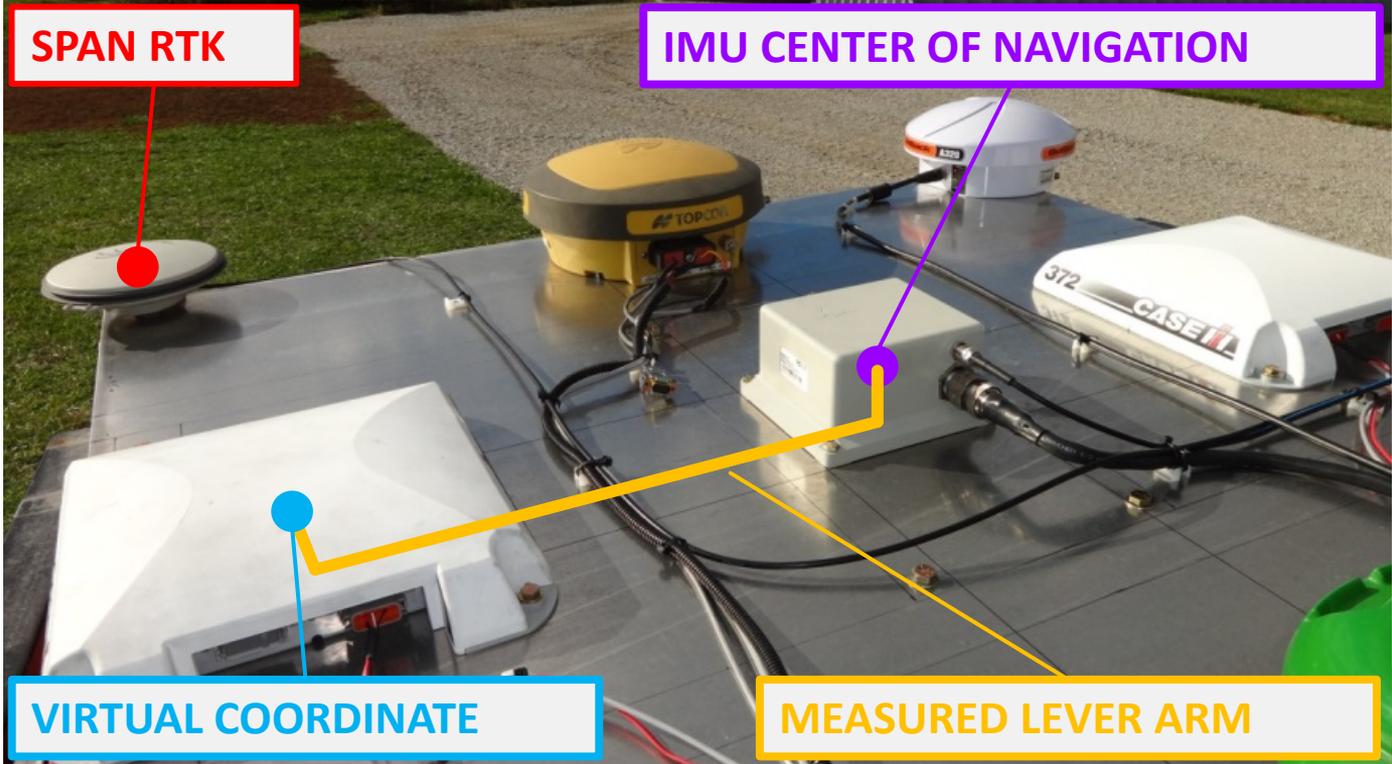
Thomas Morley

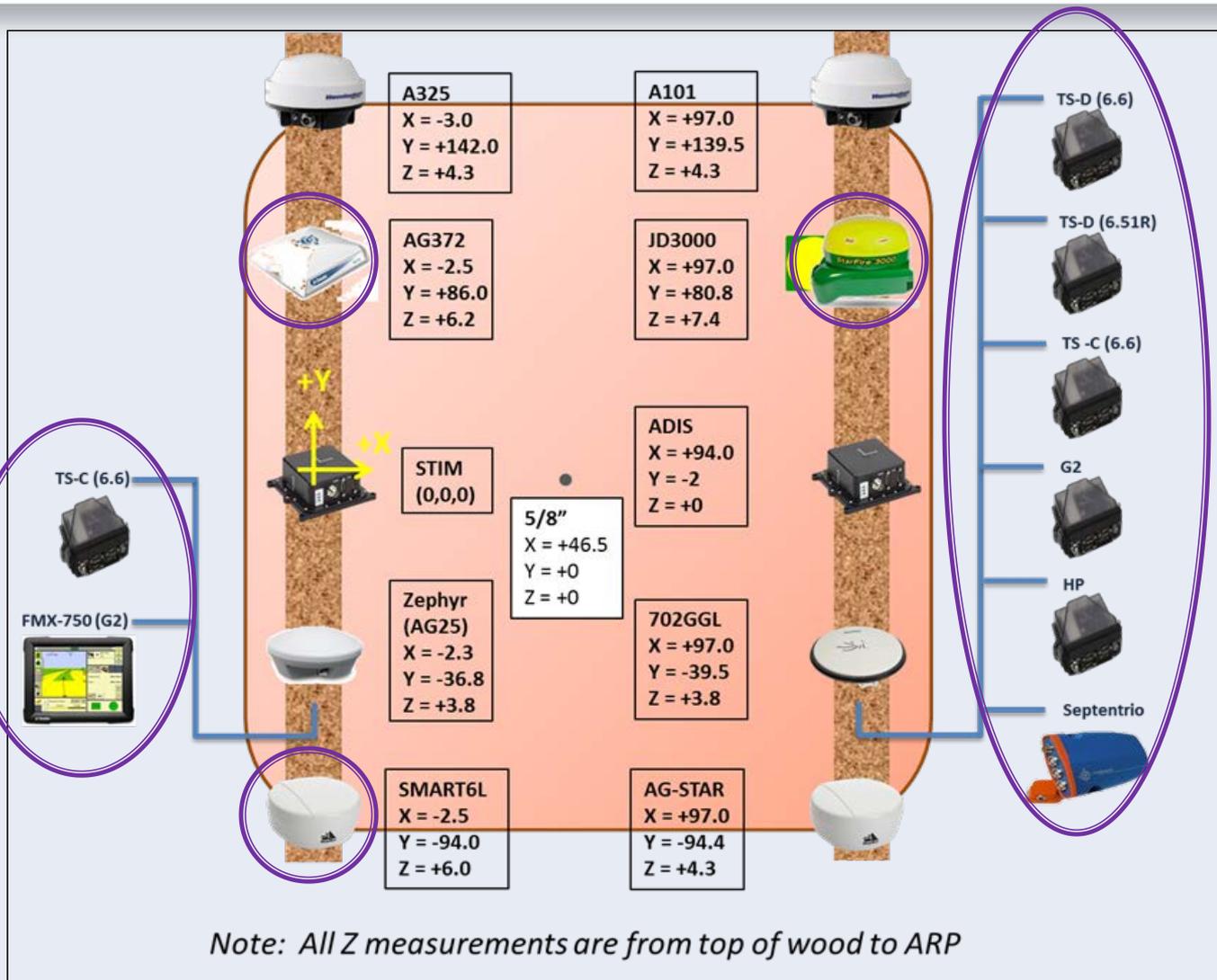
Real World Evaluation of PPP

- Actual antenna motion versus processing technique
- Dynamic evaluation methodology
- Real-world results – dynamic antennas
 - Open sky conditions
 - Operation near trees
 - Partial obstructions
 - Operation near and through a 625m long tunnel
 - Complete obstruction for 30 seconds

Processing Technique	<i>Kinematic</i>		
	<i>Static</i>		
		<i>Stationary</i>	<i>Dynamic</i>

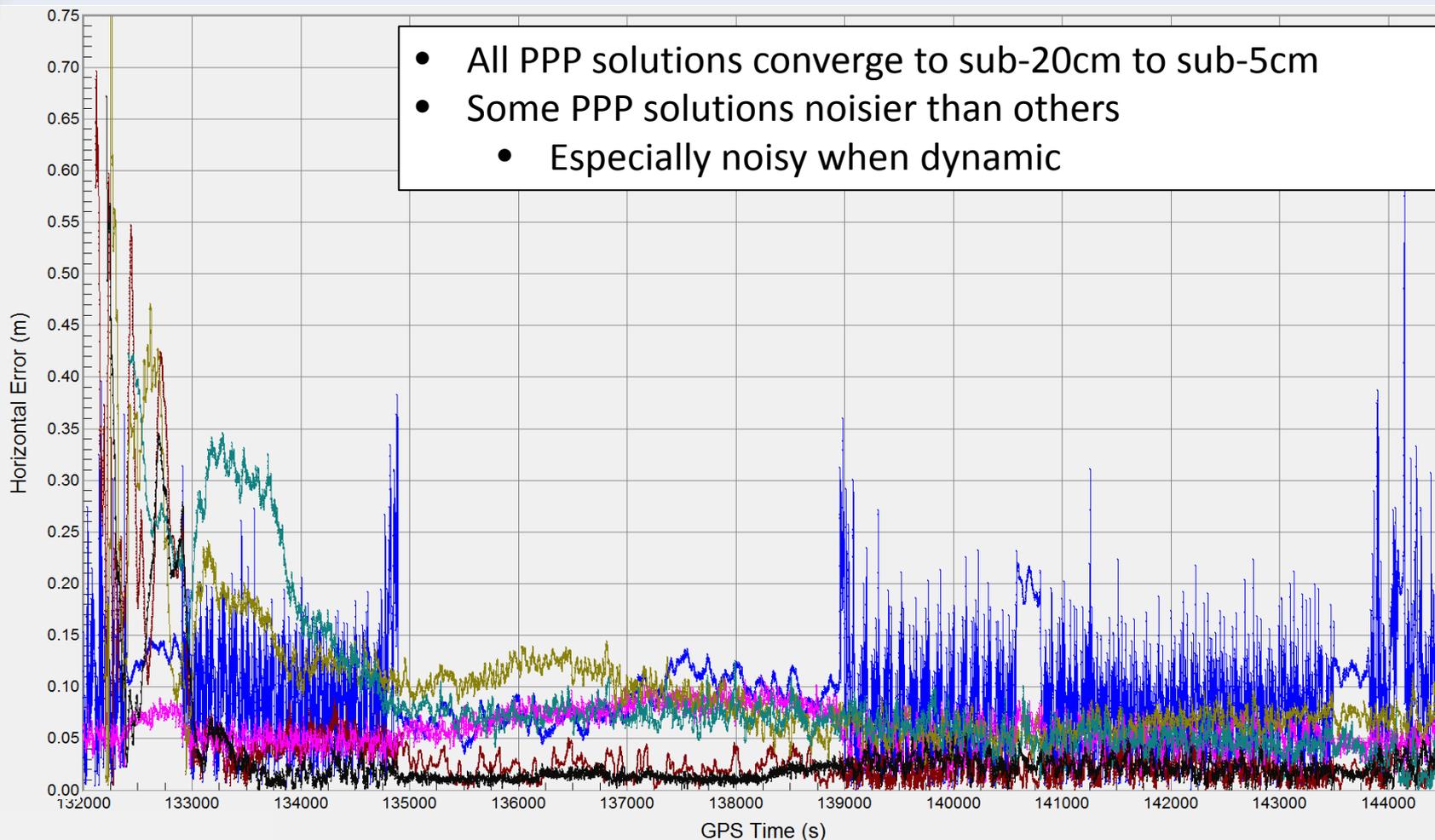
Actual Motion of Antenna

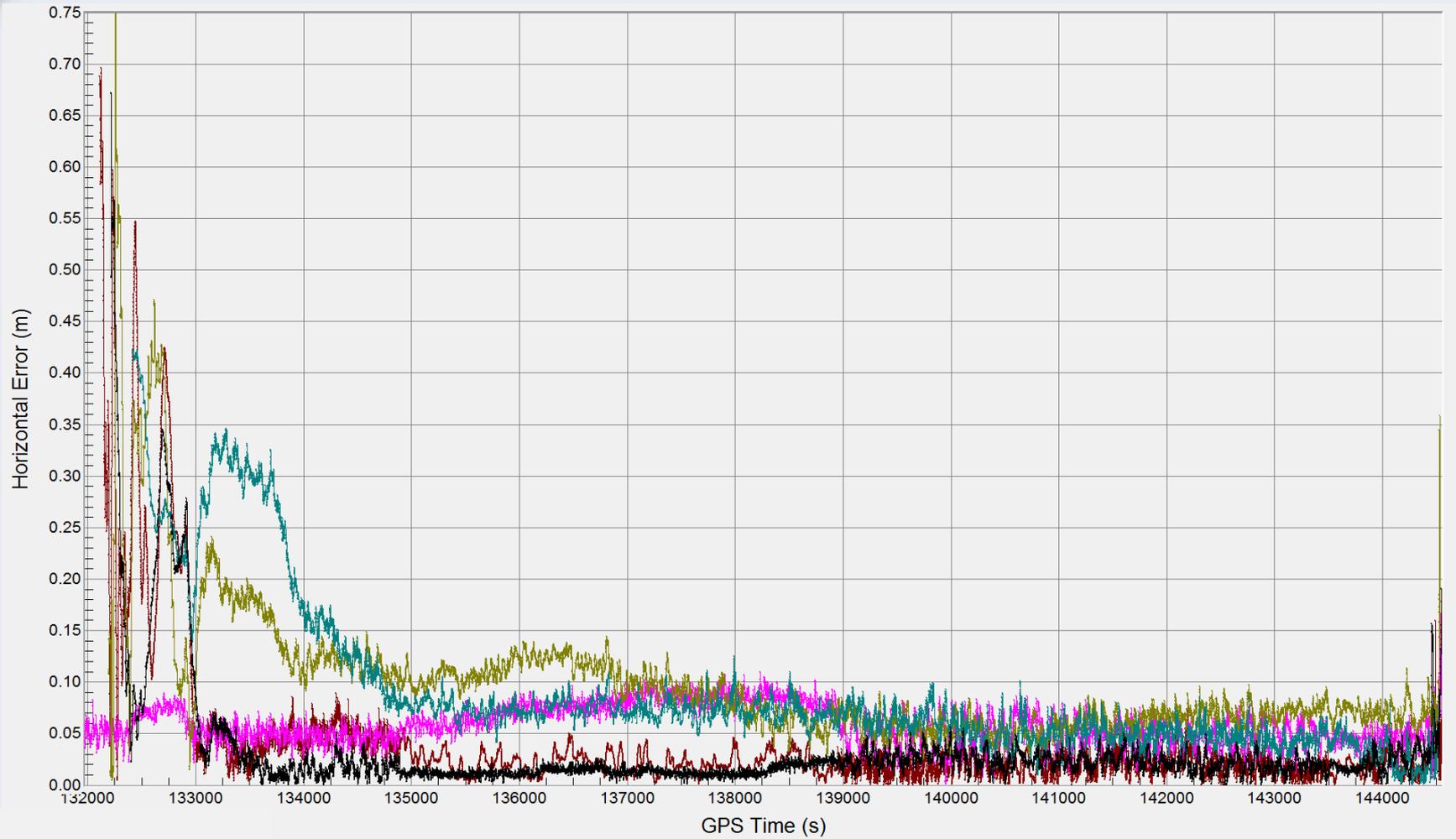




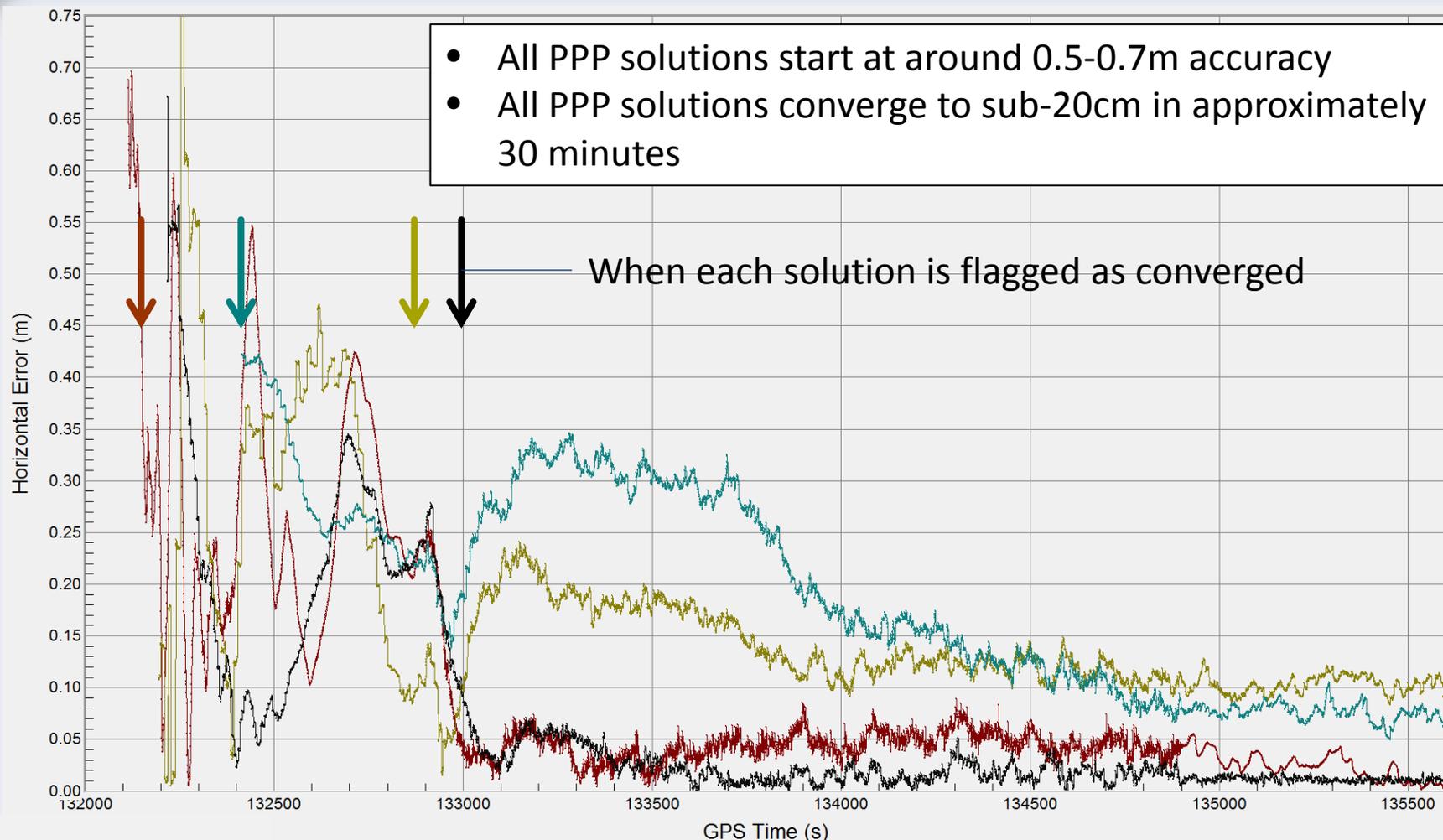


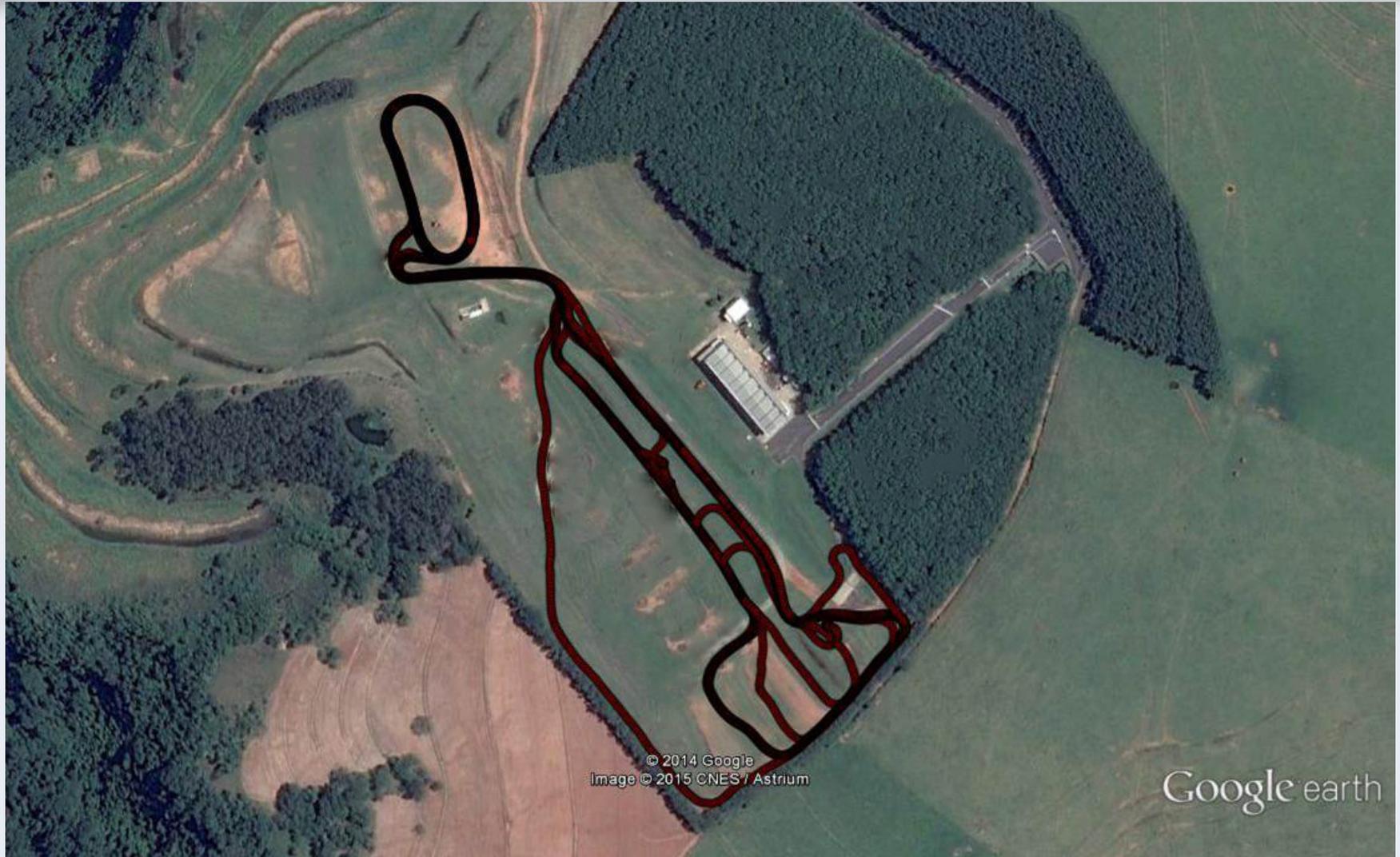
- All PPP solutions converge to sub-20cm to sub-5cm
- Some PPP solutions noisier than others
 - Especially noisy when dynamic



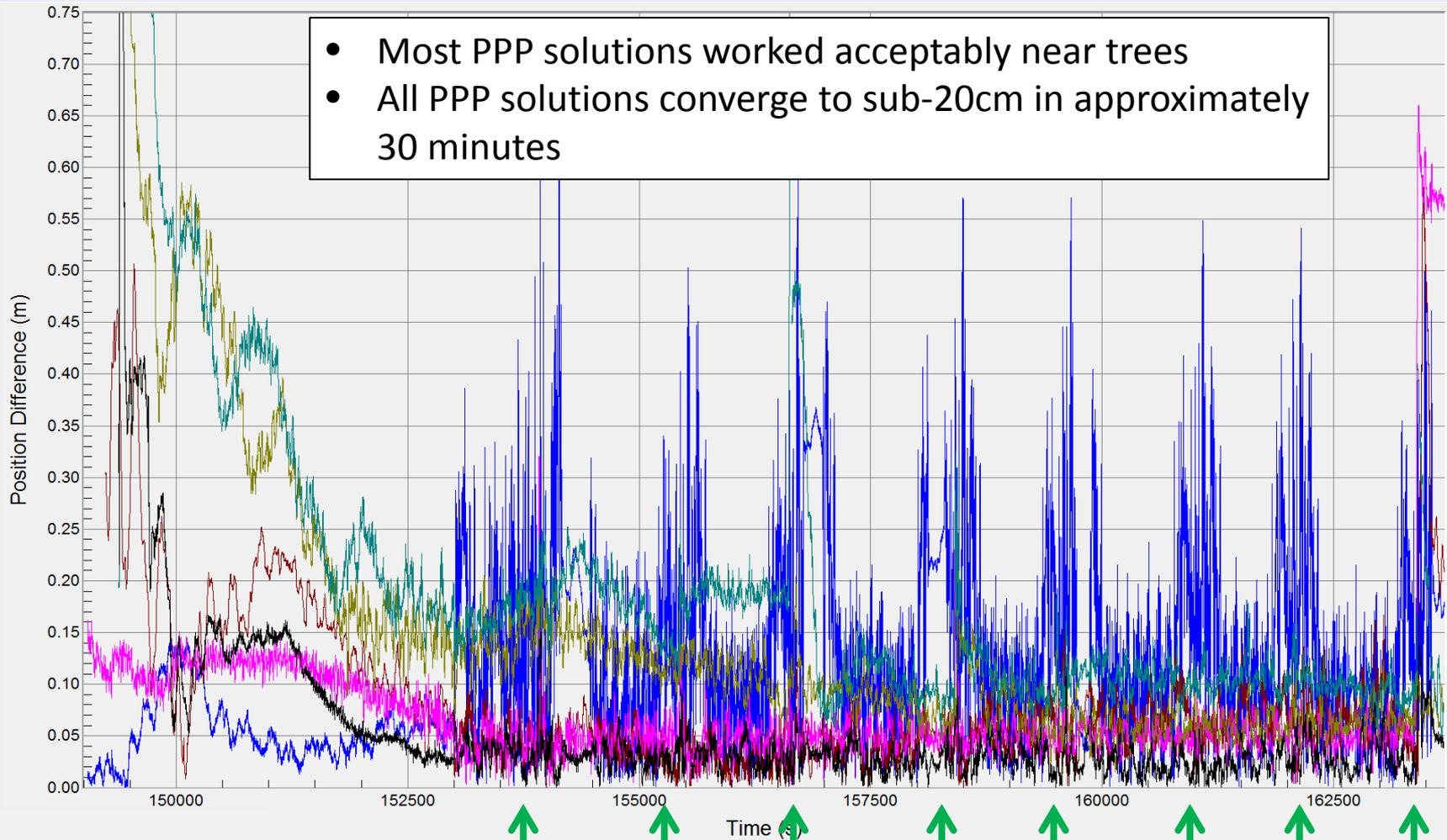


- All PPP solutions start at around 0.5-0.7m accuracy
- All PPP solutions converge to sub-20cm in approximately 30 minutes

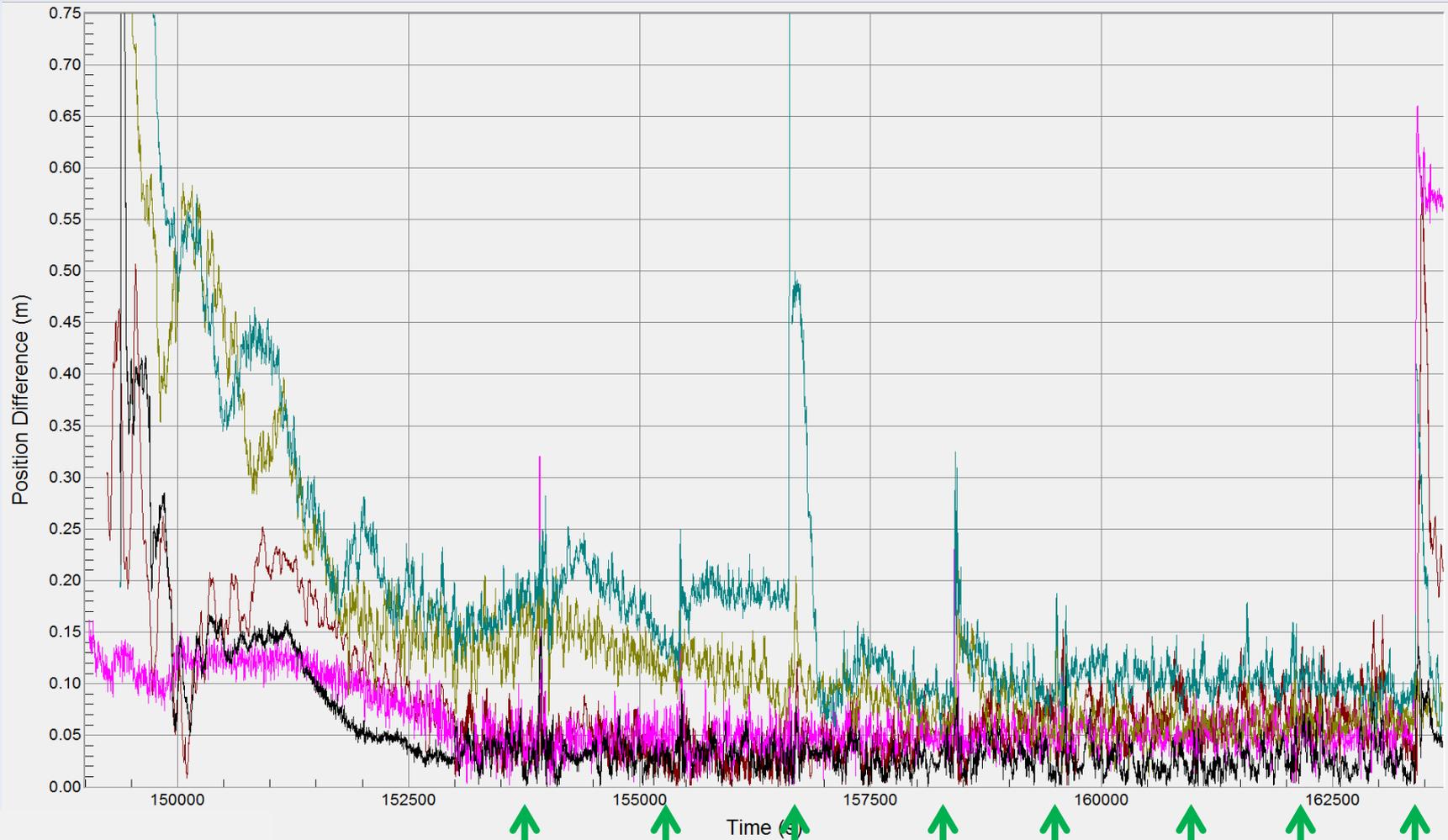




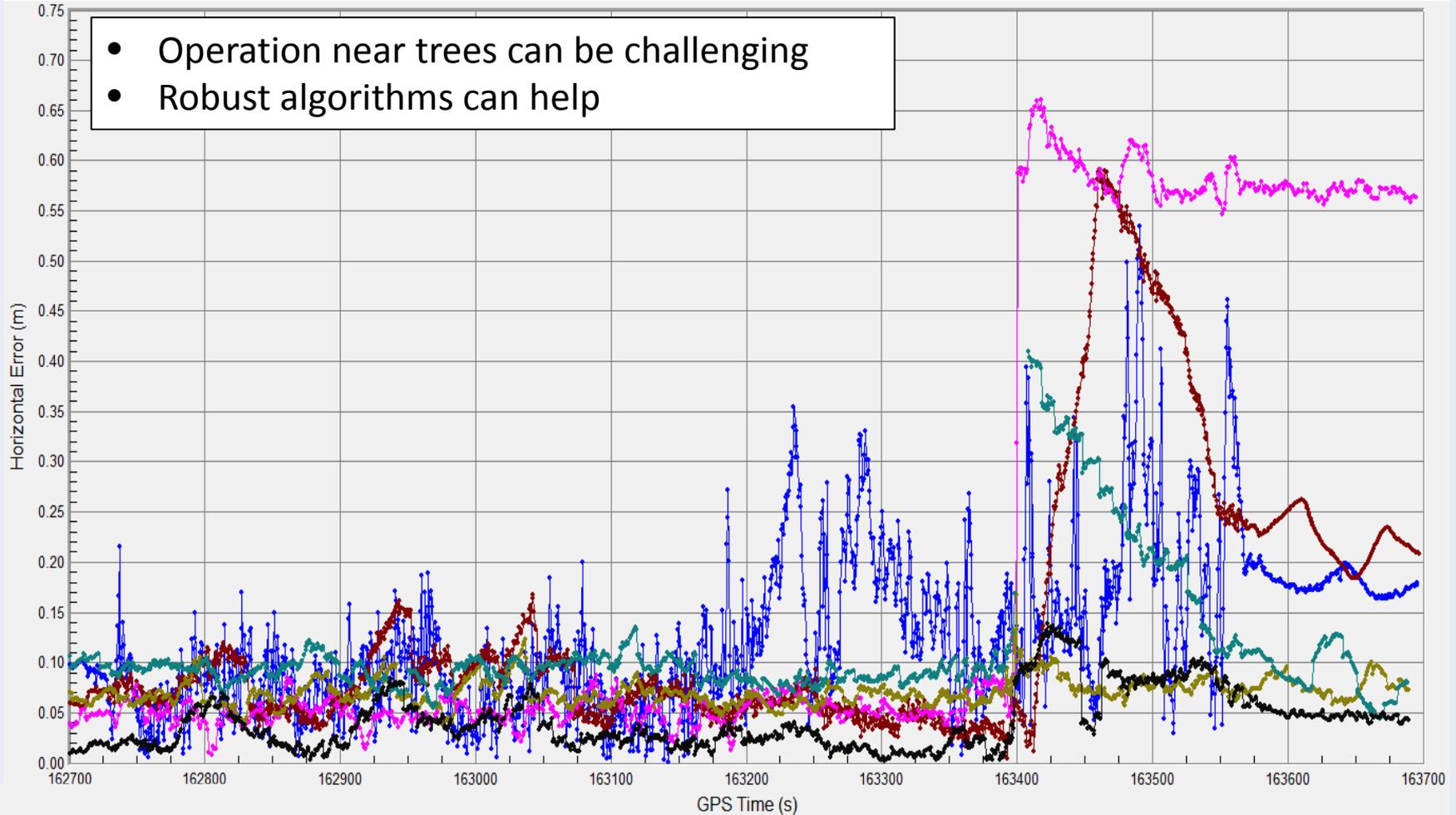
- Most PPP solutions worked acceptably near trees
- All PPP solutions converge to sub-20cm in approximately 30 minutes



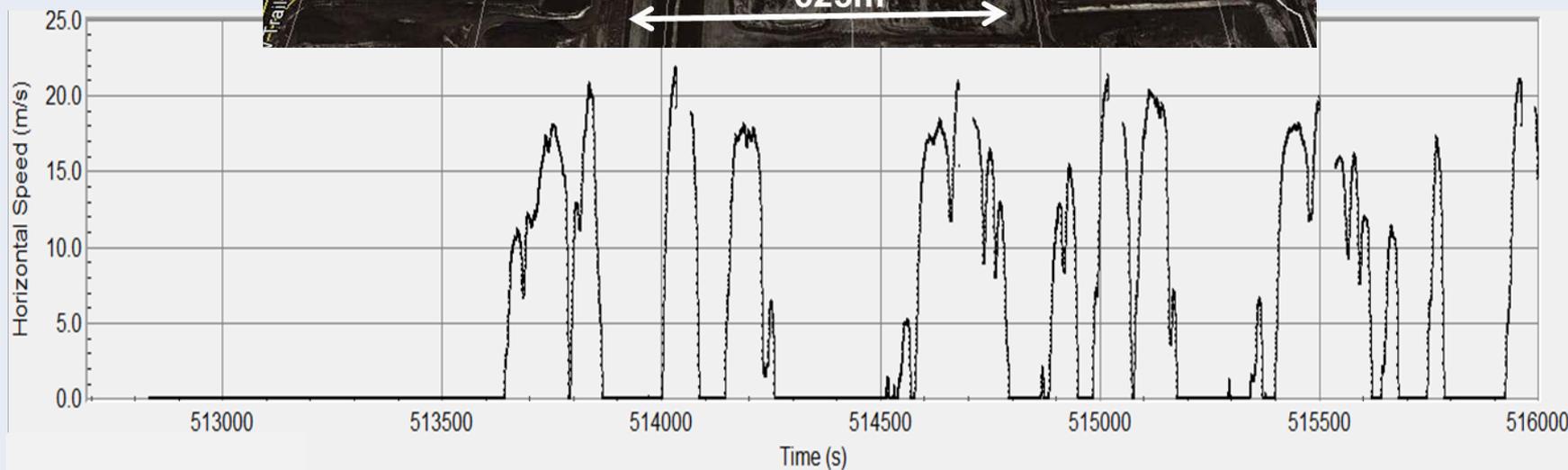
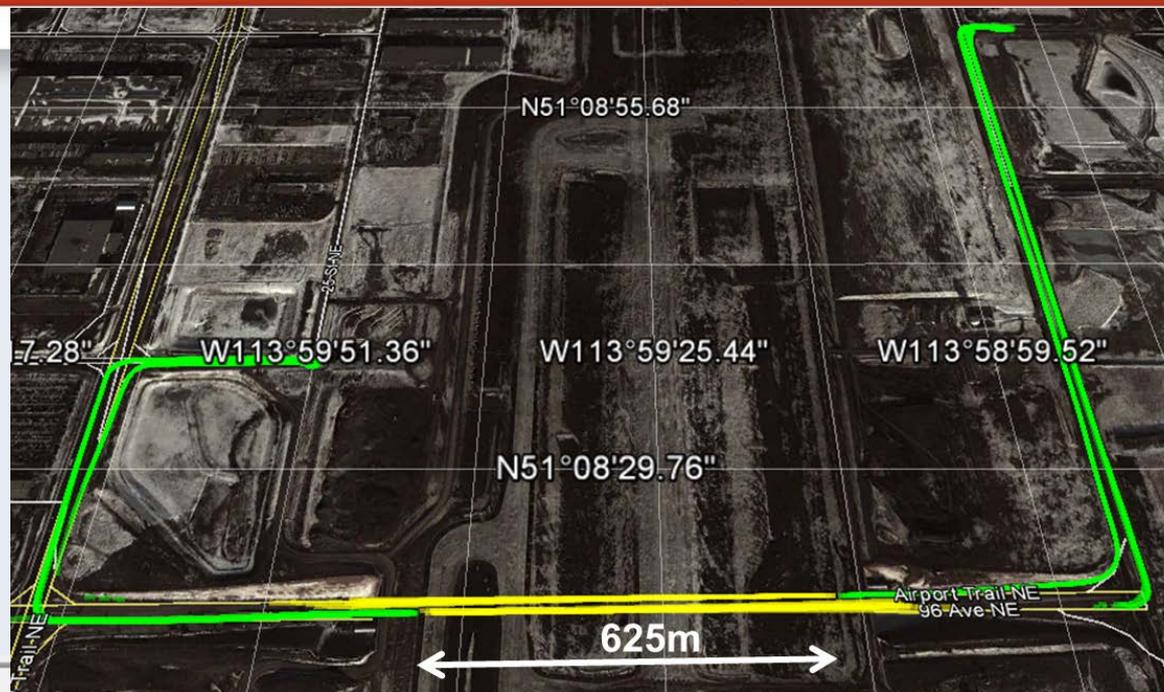
Operation near trees

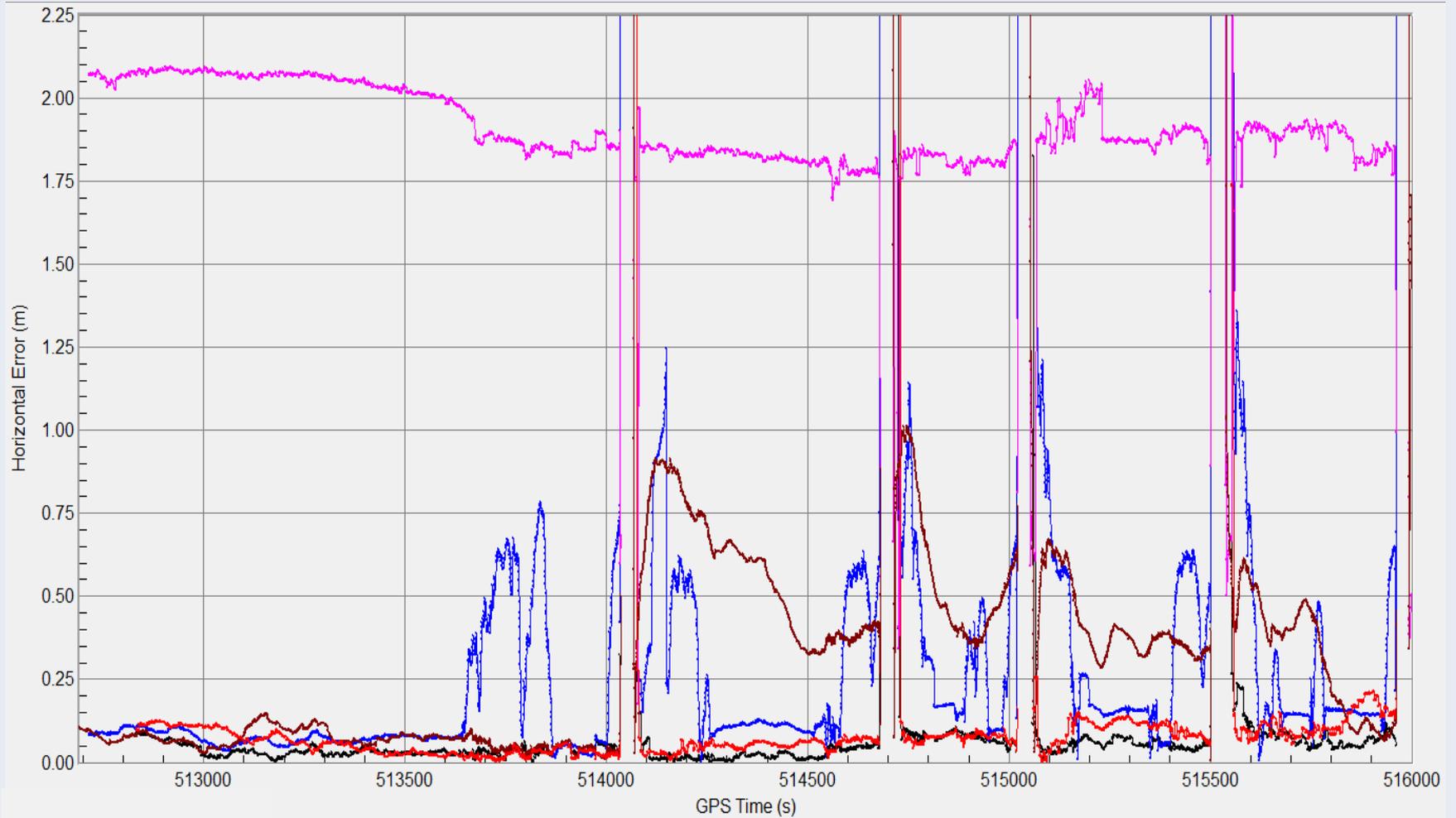


Operation near trees



Dynamic Evaluation – Horizontal Speed (Tunnel)





- Initial PPP convergence to dm accuracy can take tens of minutes
- Rapid reconvergence can occur with some flavors or implementations of PPP
- Dynamic performance of PPP is typically quite good
 - Based on many days of testing in real-world conditions
 - 6-8 different PPP solutions evaluated concurrently
 - Some solutions noisier than others, especially when dynamic
 - Most solutions can provide a reliable decimeter-level solution
 - Operation near trees can be challenging
 - Reconvergence performance can vary considerably after signal tracking disruption

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- Ensuring your success.
- Thanks for participating in today's webinar.

Poll #3

Based on what you have heard today, in my applications I plan to:

- Consider replacing a meter level solution with PPP
- Consider replacing RTK with PPP
- I have no need for PPP
- Continue to use both RTK and PPP
- Not sure. I will wait.

Ask the Experts – Part 2



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Thank you!



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